



Telekomunikaciona merenja TM P07 2018

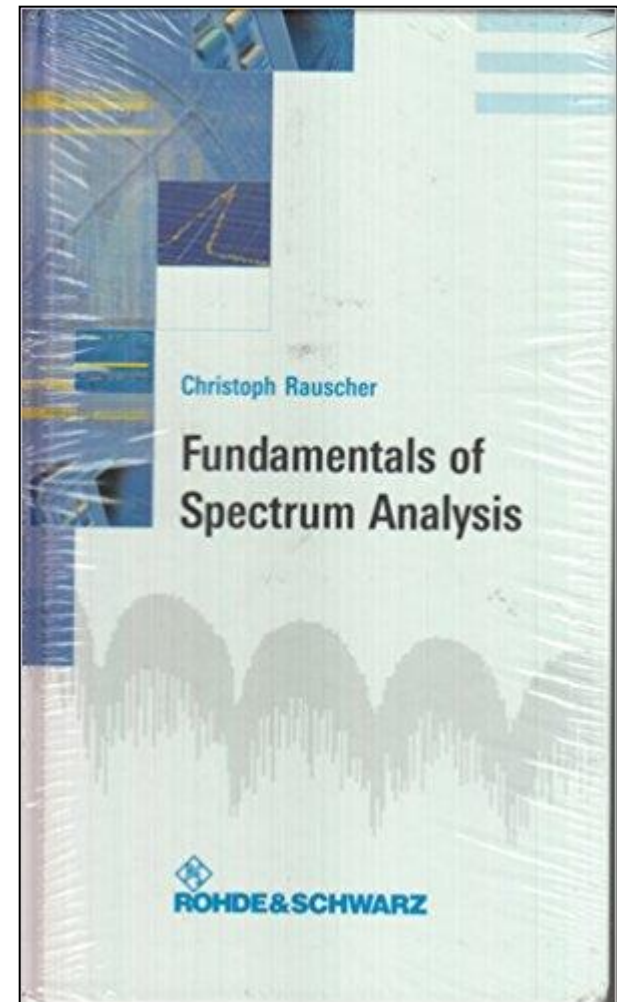
Profesor dr Miroslav Lutovac

"This project has been funded with support from the European Commission. This publication [communication] reflects the views only of the author, and the Commission cannot be held responsible for any use which may be made of the information contained therein"

Osnove analize spektra

Rauscher C.,
Fundamentals of Spectrum
Analysis,
Rohde & Schwarz, 2006

Poglavlje 5



Performanse analizatora spektra

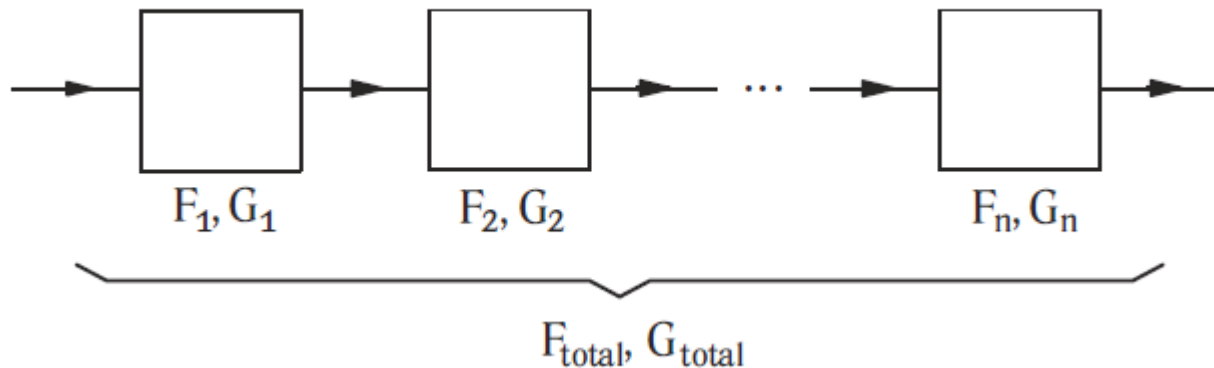
- **Sopstveni šum**
- Termički šum u prijemniku i analizatoru spektra
- Dovodi do redukcije S/N
- Sopstveni šum je mera osetljivosti analizatora spektra
- To je minimalni nivo ulaznog signala koji može da se detektuje
- Bezdimenziona mera, faktor šuma F , mreže sa dva pristupa je odnos između S/N na ulaznom i izlaznom portu mreže

$$F = \frac{S_1/N_1}{S_2/N_2}$$

$$\begin{aligned} S_1/N_1 &= \text{signal-to-noise ratio at the input of the network} \\ S_2/N_2 &= \text{signal-to-noise ratio at the output of the network} \end{aligned}$$

$$NF = 10 \cdot \log F$$

Kakadna veza

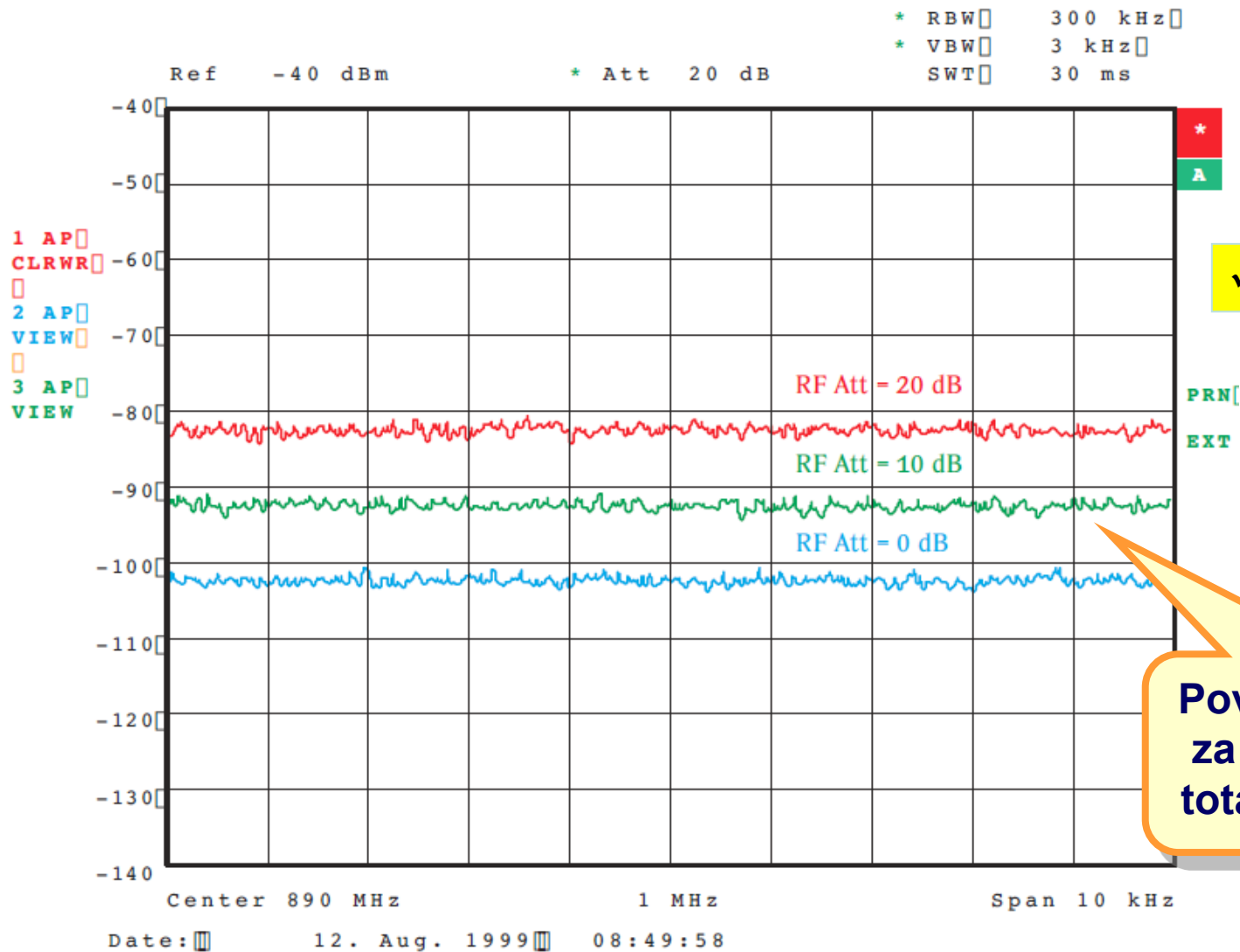


$$F_{total} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 \cdot G_2} + \dots + \frac{F_n - 1}{\prod_{i=1}^{n-1} G_i}$$

F_i = noise factor of an individual stage

G_i = gain of an individual stage

Usrednjen šum i RF slabljenje



✓ Gausov šum

Povećanje slabljenja
za 10 dB, povećava
totalni šum za 10 dB

Prikazani srednji šum

- Spektralna gustina šuma je konstantna u opsegu

$$L_{\text{DAN}} = 10 \cdot \log \left(\frac{k \cdot T \cdot B_{\text{N,IF}}}{1 \cdot 10^{-3} \text{ W}} \right) + NF_{\text{SA}} - 2.5 \text{ dB}$$

L_{DAN} = displayed average noise level, in dBm

k = Boltzmann's constant, $k = 1.38 \cdot 10^{-23} \text{ W/Hz}$

T = ambient temperature, in K

$B_{\text{N,IF}}$ = noise bandwidth of IF filter

NF_{SA} = noise figure of spectrum analyzer, in dB

-2.5 dB = underweighting of noise by sample detector ;
averaging of logarithmic level values

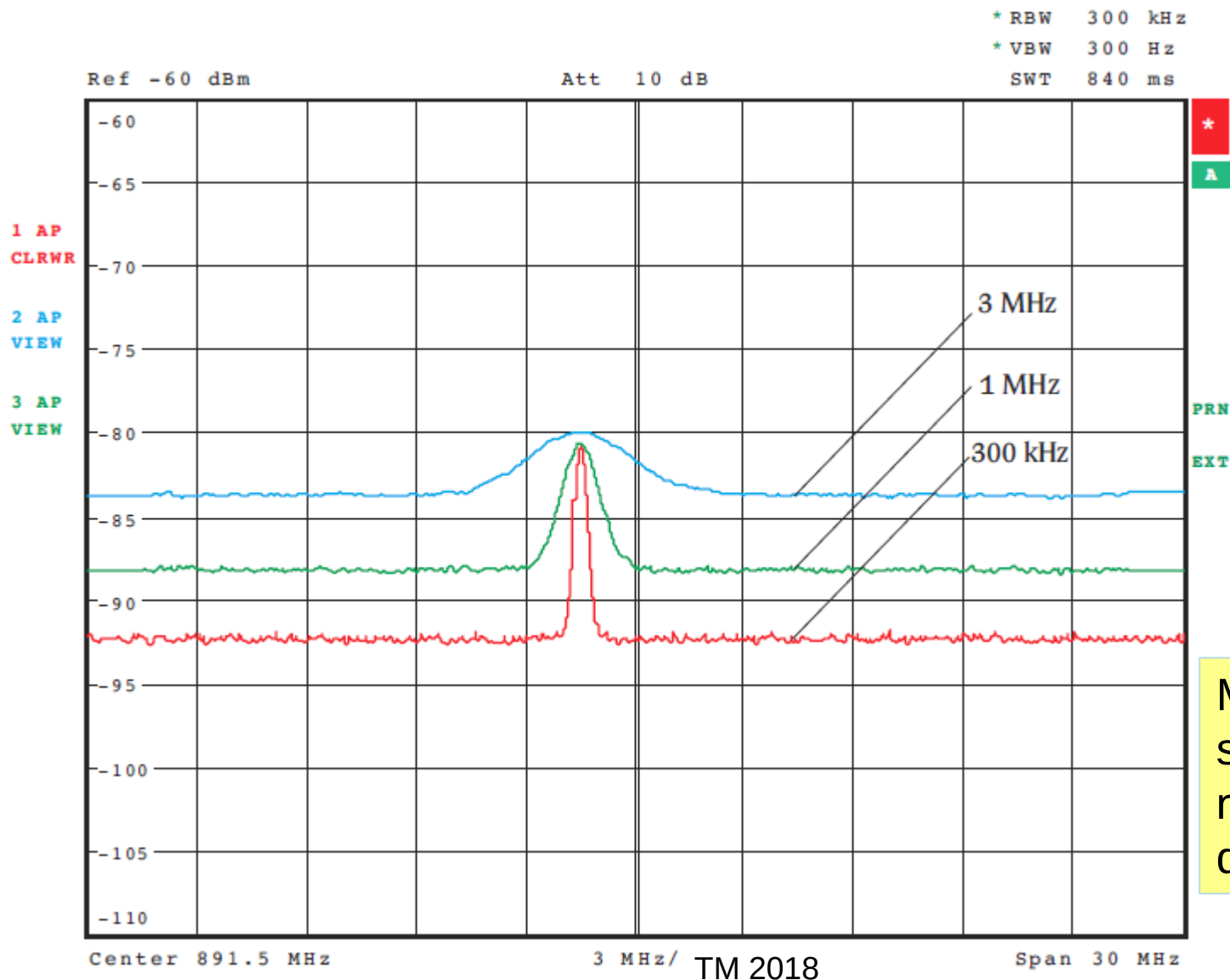
-174 dBm (1 Hz)
odgovara
raspoloživom
termičkom šumu.

Snaga na otpornosti u
opsegu 1 Hz na
temperaturi 290 K

ambient temperature of 290 K

$$L_{\text{DAN}} = -174 \text{ dBm (1 Hz)} + \left(10 \cdot \log \frac{B_{\text{N,IF}}}{\text{Hz}} \right) \text{ dB} + NF_{\text{SA}} - 2.5 \text{ dB}$$

Usrednjen nivo šuma za razne opsege



Tipične specifikacije šuma koji može da se prikaže na analizatoru spektra

usrednjavanje

Displayed average noise level

(0 dB RF attenuation, RBW 10 Hz, VBW 1 Hz, 20 averages, trace average, span 0 Hz, termination 50 Ω)

Frequency

9 kHz	<-95 dBm
100 kHz	<-100 dBm
1 MHz	<-120 dBm, typ. -125 dBm
10 MHz to 7 GHz	<-138 dBm, typ. -143 dBm

Nelinearnost

- Distorzija signala od ulaza do izlaza mreže sa dva pristupa
- Samo kada se koriste aktivne komponente:
 - pojačavač, mikser - mešač

$$v_{out}(t) = G_V \cdot v_{in}(t)$$

$v_{out}(t)$ = voltage at output of network

$v_{in}(t)$ = voltage at input of network

G_V = voltage gain of network

$$v_{out}(t) = \sum_{n=1}^{\infty} a_n \cdot v_{in}^n(t) = a_1 \cdot v_{in}(t) + a_2 \cdot v_{in}^2(t) + a_3 \cdot v_{in}^3(t) + \dots$$

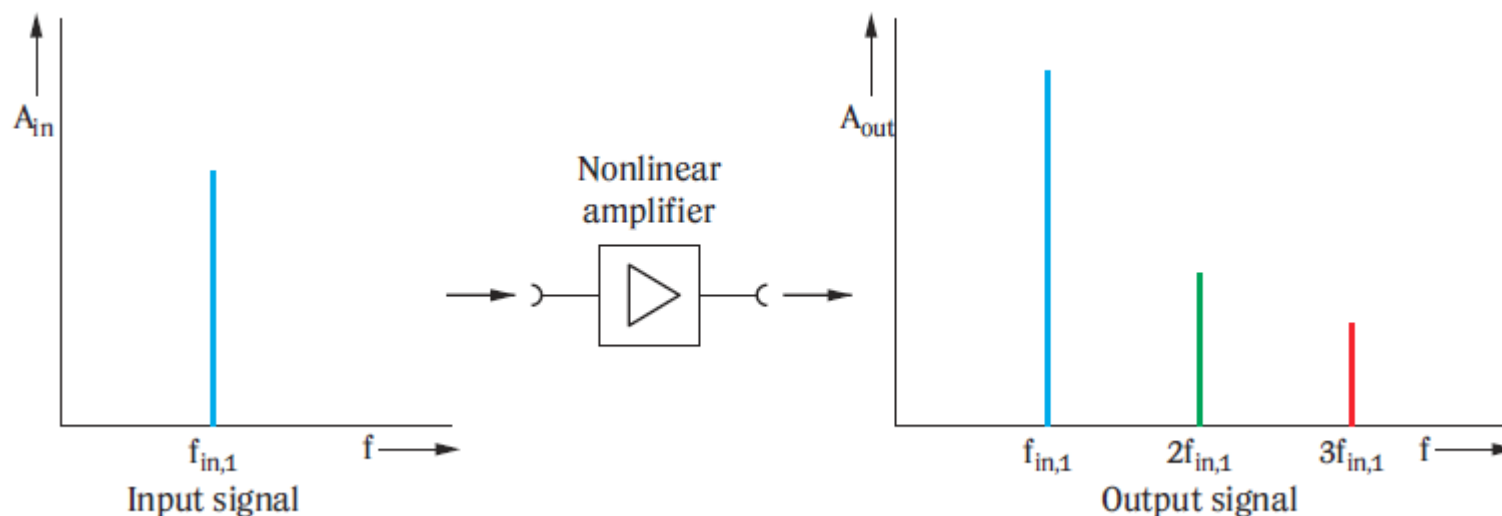
$v_{out}(t)$ = voltage at output of network

$v_{in}(t)$ = voltage at input of network

a_n = coefficient of nonlinear element of voltage gain

U praksi do 3. stepena

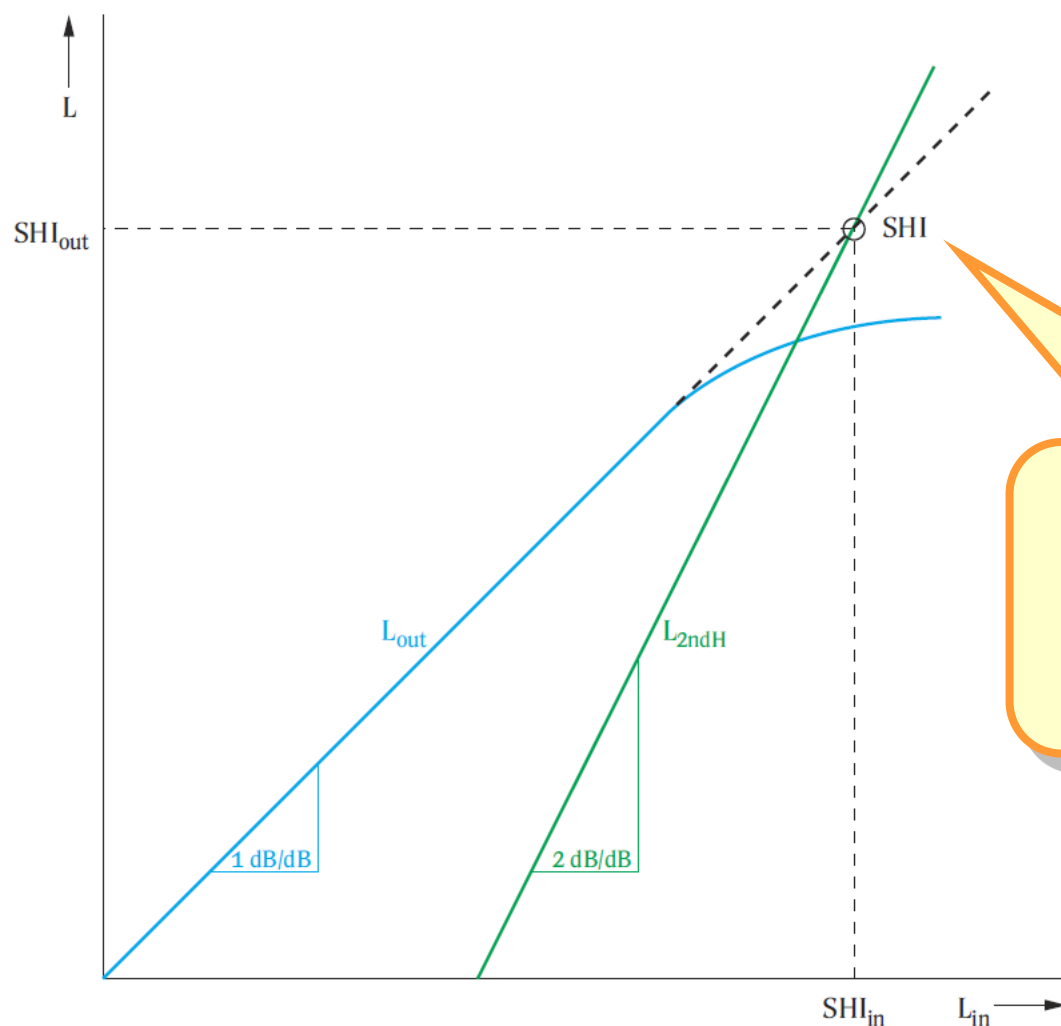
Pobuda sa 1 sinusoidom



3. harmonik

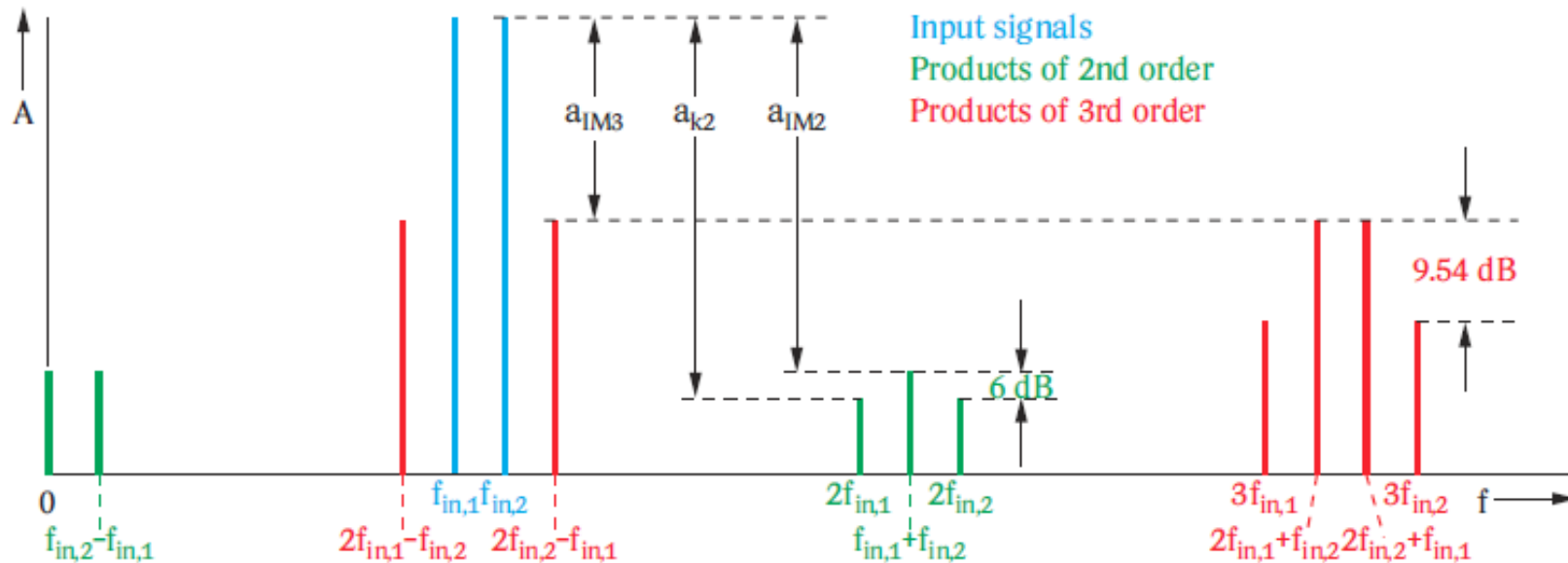
Kada je nivo signala veći, ima više harmonika

Drugi harmonik



Presečna tačka kada drugi harmonik ima isti nivo kao osnovni signal

Sa dve sinusoide

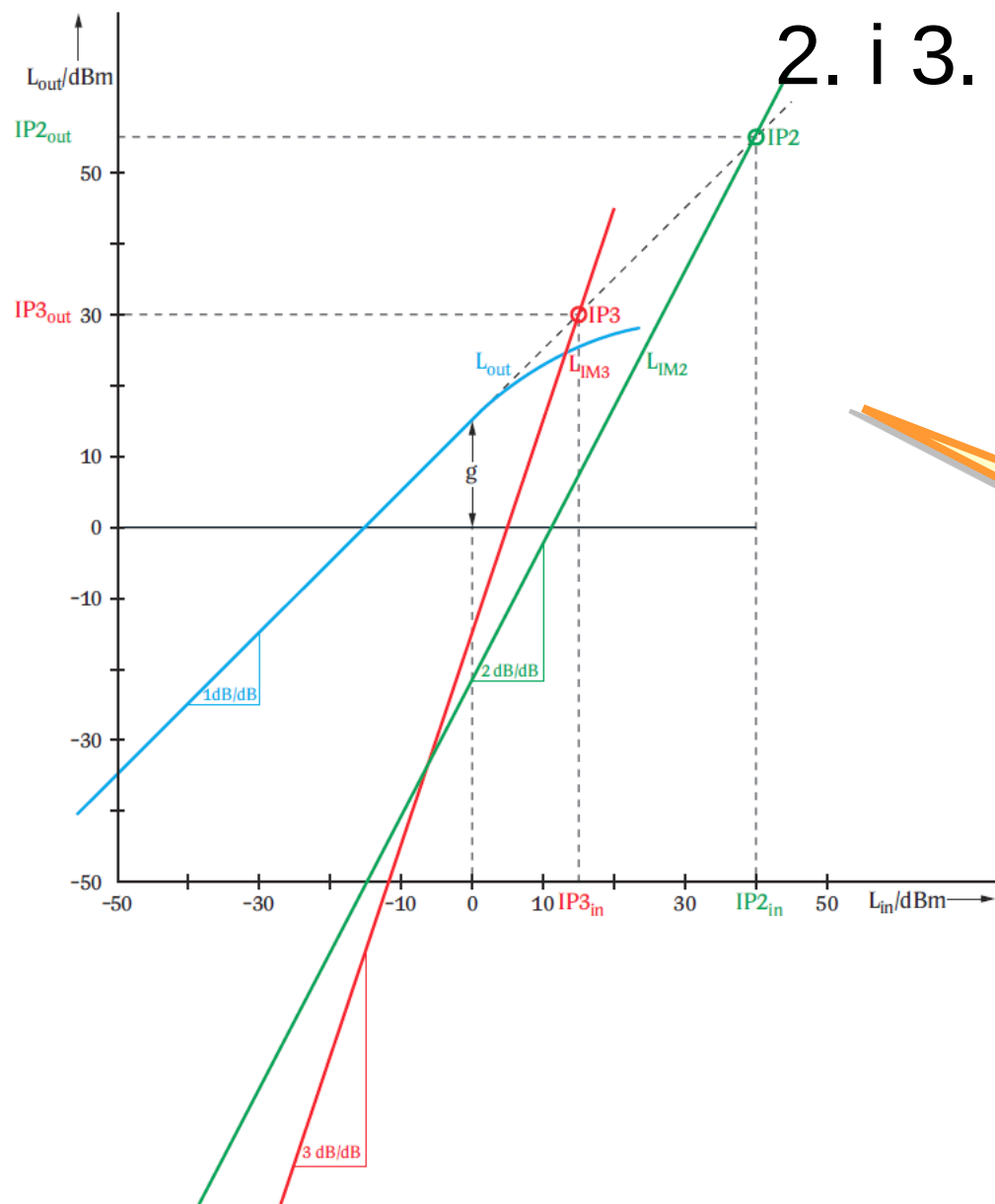


Intermodulacioni produkti

Sa dve sinusoide

DC component	$a_2 \cdot 0.5 (\hat{U}_{in,1}^2 + \hat{U}_{in,2}^2)$
Fundamentals	$a_1 \cdot \hat{U}_{in,1} \cdot \sin(\omega_1 t)$ $a_1 \cdot \hat{U}_{in,2} \cdot \sin(\omega_2 t)$
2nd harmonics	$a_2 \cdot 0.5 \cdot \hat{U}_{in,1}^2 \cdot \cos(2 \cdot \omega_1 t)$ $a_2 \cdot 0.5 \cdot \hat{U}_{in,2}^2 \cdot \cos(2 \cdot \omega_2 t)$
Intermodulation products of 2nd order	$a_2 \cdot \hat{U}_{e,1} \cdot \hat{U}_{in,2} \cdot \cos(\omega_1 - \omega_2)t$ $a_2 \cdot \hat{U}_{e,1} \cdot \hat{U}_{in,2} \cdot \cos(\omega_1 + \omega_2)t$
3rd harmonics	$a_3 \cdot 0.25 \cdot \hat{U}_{in,1}^3 \cdot \sin(3 \cdot \omega_1 t)$ $a_3 \cdot 0.25 \cdot \hat{U}_{in,2}^3 \cdot \cos(3 \cdot \omega_2 t)$
Intermodulation products of 3rd order	$a_3 \cdot \hat{U}_{in,1}^2 \cdot \hat{U}_{in,2} \cdot 0.75 \cdot \sin(2\omega_1 + \omega_2)t$ $a_3 \cdot \hat{U}_{in,1}^2 \cdot \hat{U}_{in,2} \cdot 0.75 \cdot \sin(2\omega_2 + \omega_1)t$ $a_3 \cdot \hat{U}_{in,1}^2 \cdot \hat{U}_{in,2} \cdot 0.75 \cdot \sin(2\omega_1 - \omega_2)t$ $a_3 \cdot \hat{U}_{in,1}^2 \cdot \hat{U}_{in,2} \cdot 0.75 \cdot \sin(2\omega_2 - \omega_1)t$

2. i 3. harmonik



Presečne tačke

Tipične specifikacije intermodulacije na analizatoru spektra

Intermodulation

3rd order intermodulation

Intermodulation-free dynamic range

level 2×-30 dBm, $\Delta f > 5 \cdot \text{RBW}$ or 10 kHz, whichever is the greater value

Frequency

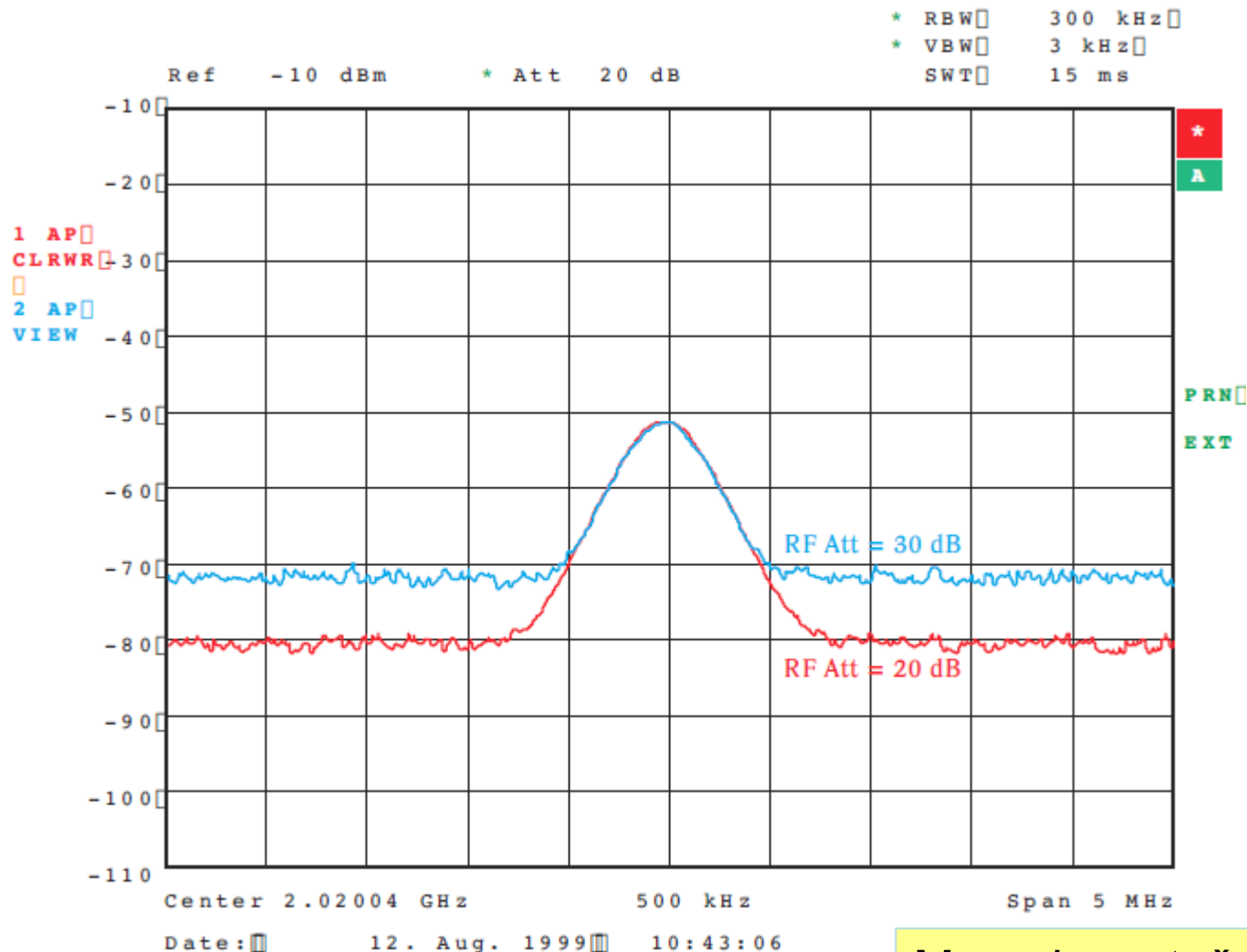
20 MHz to 200 MHz	>70 dBc, TOI >5 dBm
200 MHz to 3 GHz	>74 dBc, TOI >7 dBm
3 GHz to 7 GHz	>80 dBc, TOI >10 dBm

2nd harmonic intercept point (SHI)

Frequency <50 MHz	25 dBm
50 MHz to 3 GHz	35 dBm
3 GHz to 7 GHz	45 dBm

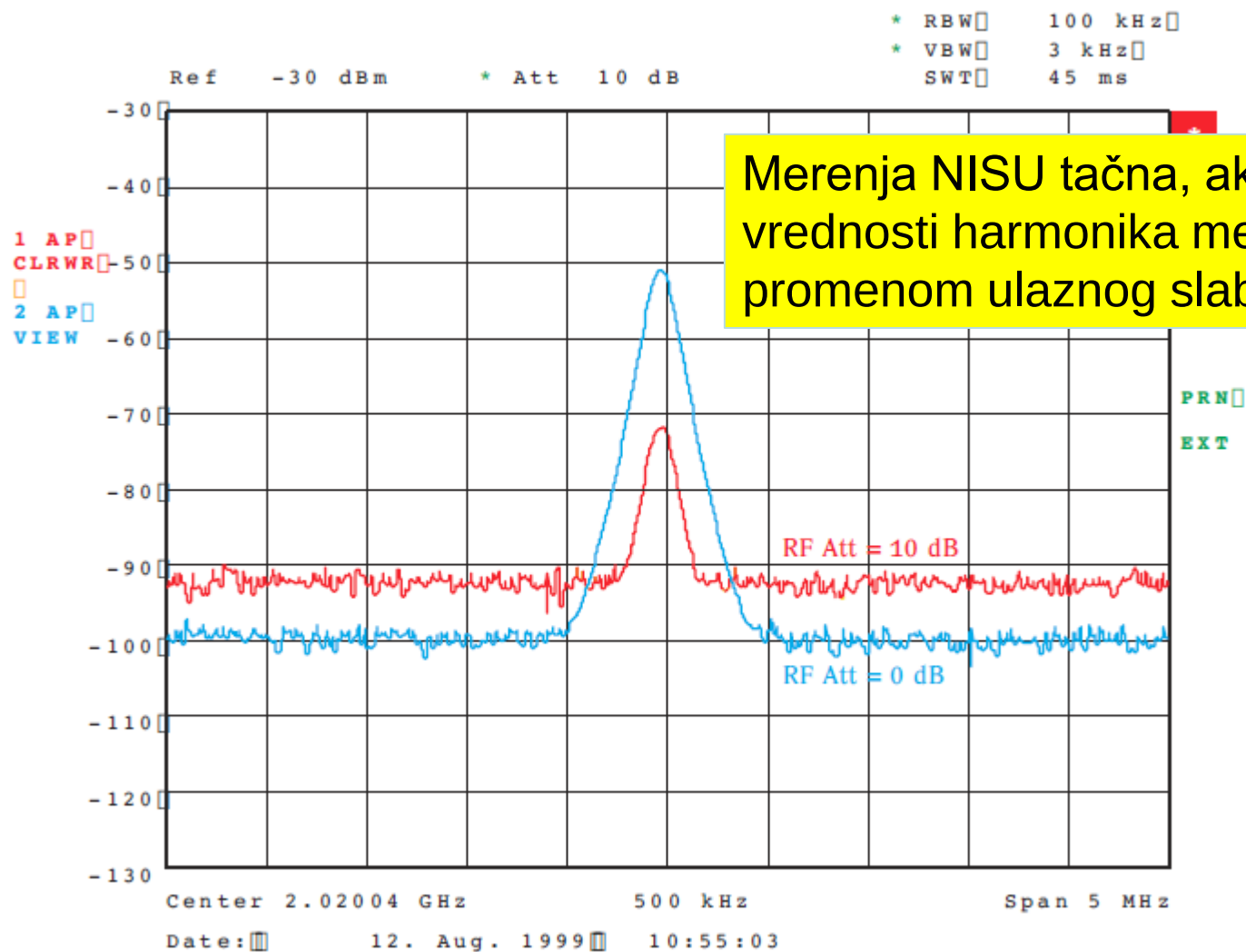
Frekvecijski
opseg
200 MHz do
3 GHz

Intermodulacioni produkti



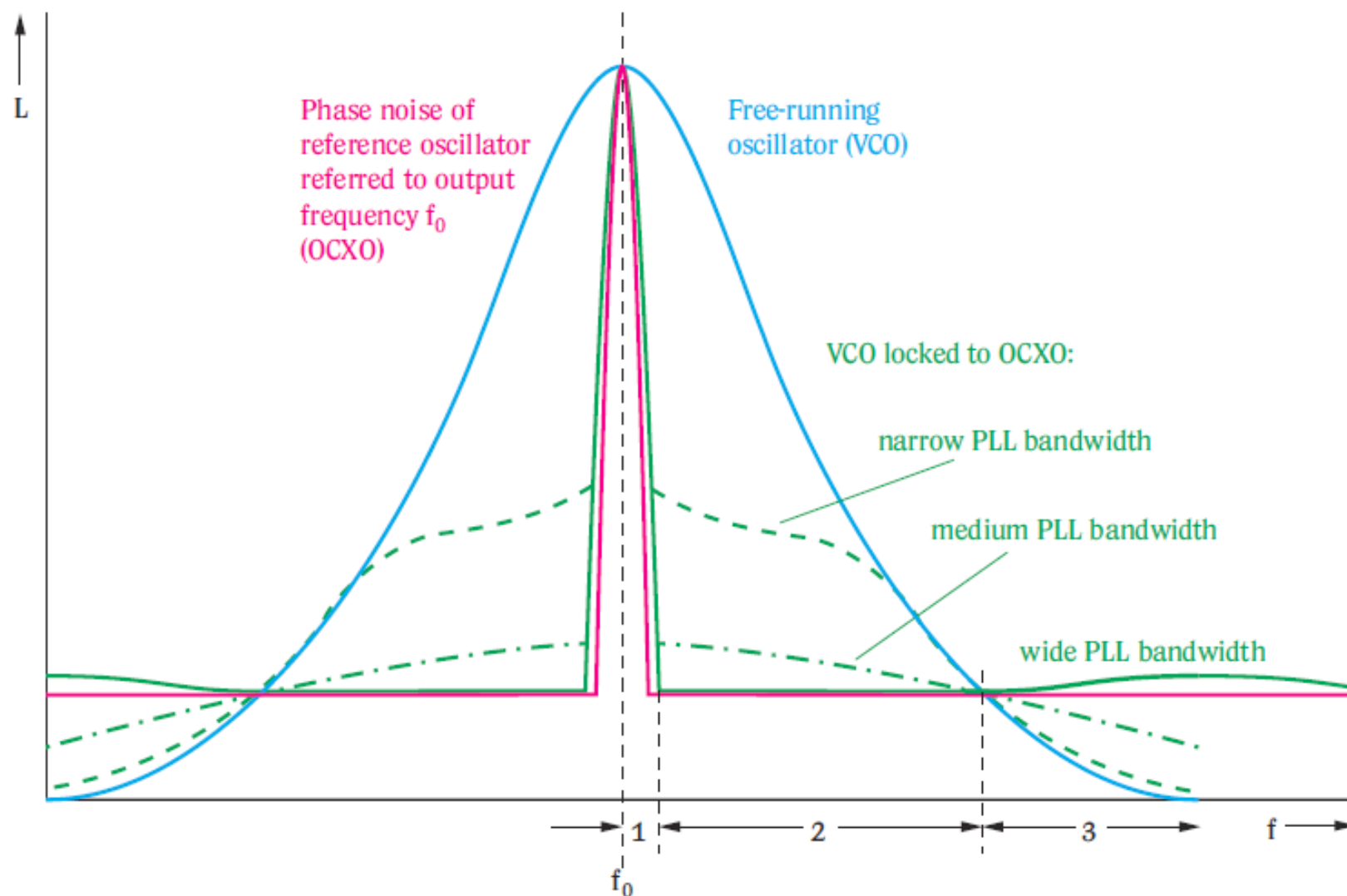
Merenja su tačna

Intermodulacioni produkti

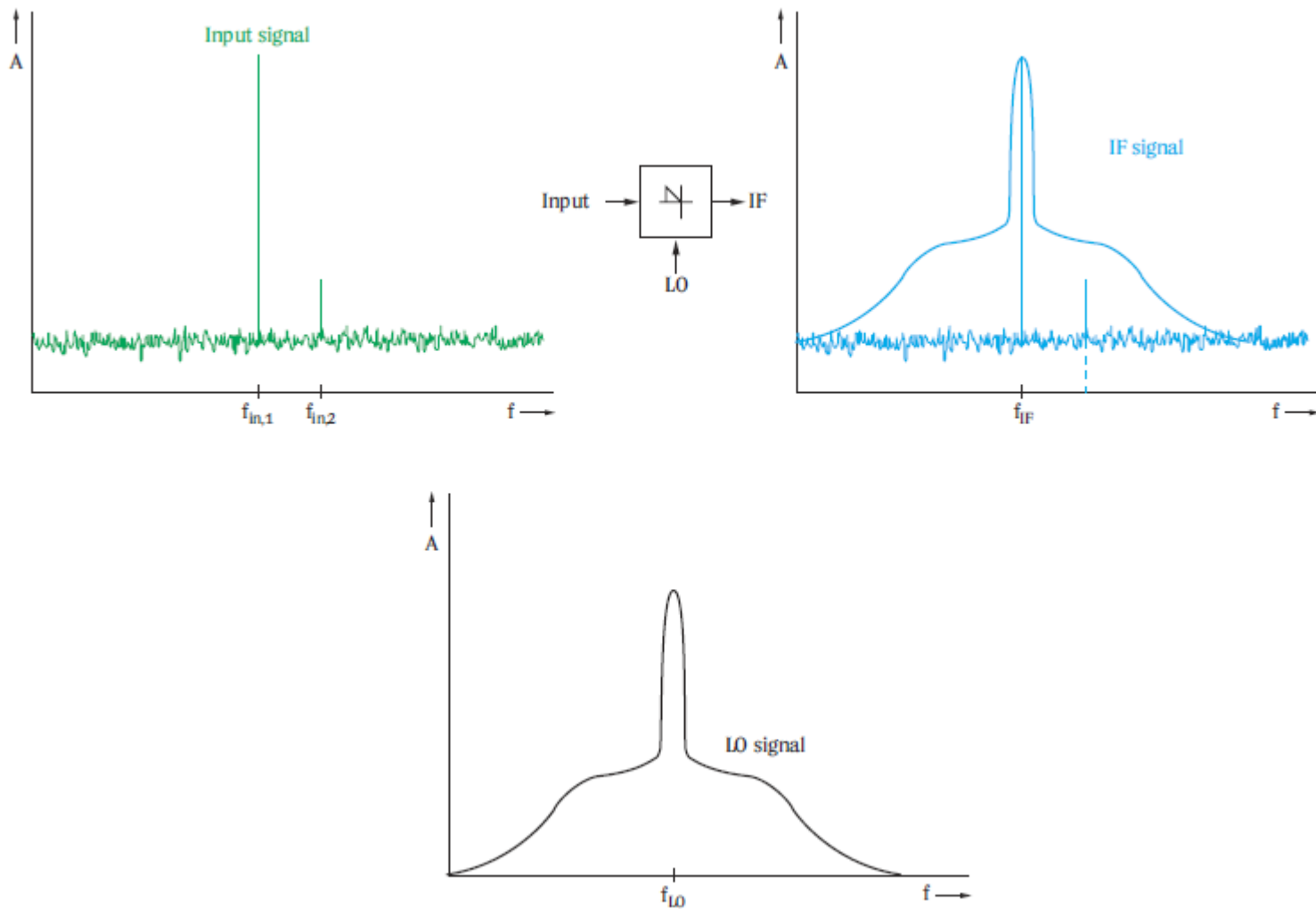


Merenja NISU tačna, ako se relativne vrednosti harmonika menja, sa promenom ulaznog slabljenja

Fazni šum



Interni fazni šum transferovan na ulazni signal recipročnim mešanjem



Tipične specifikacije faznog šuma

Spectral purity (dBc (1 Hz))
SSB phase noise, $f = 500$ MHz

Carrier offset

100 Hz	<-90. typ. -94
1 kHz	<-100. typ. -108
10 kHz	<-106. typ. -113
100 kHz ¹⁾	<-110. typ. -113
1 MHz ¹⁾	<-120. typ. -125
10 MHz	typ. -145

Residual FM

($f = 500$ MHz, RBW = 1 kHz,
sweep time 100 ms)

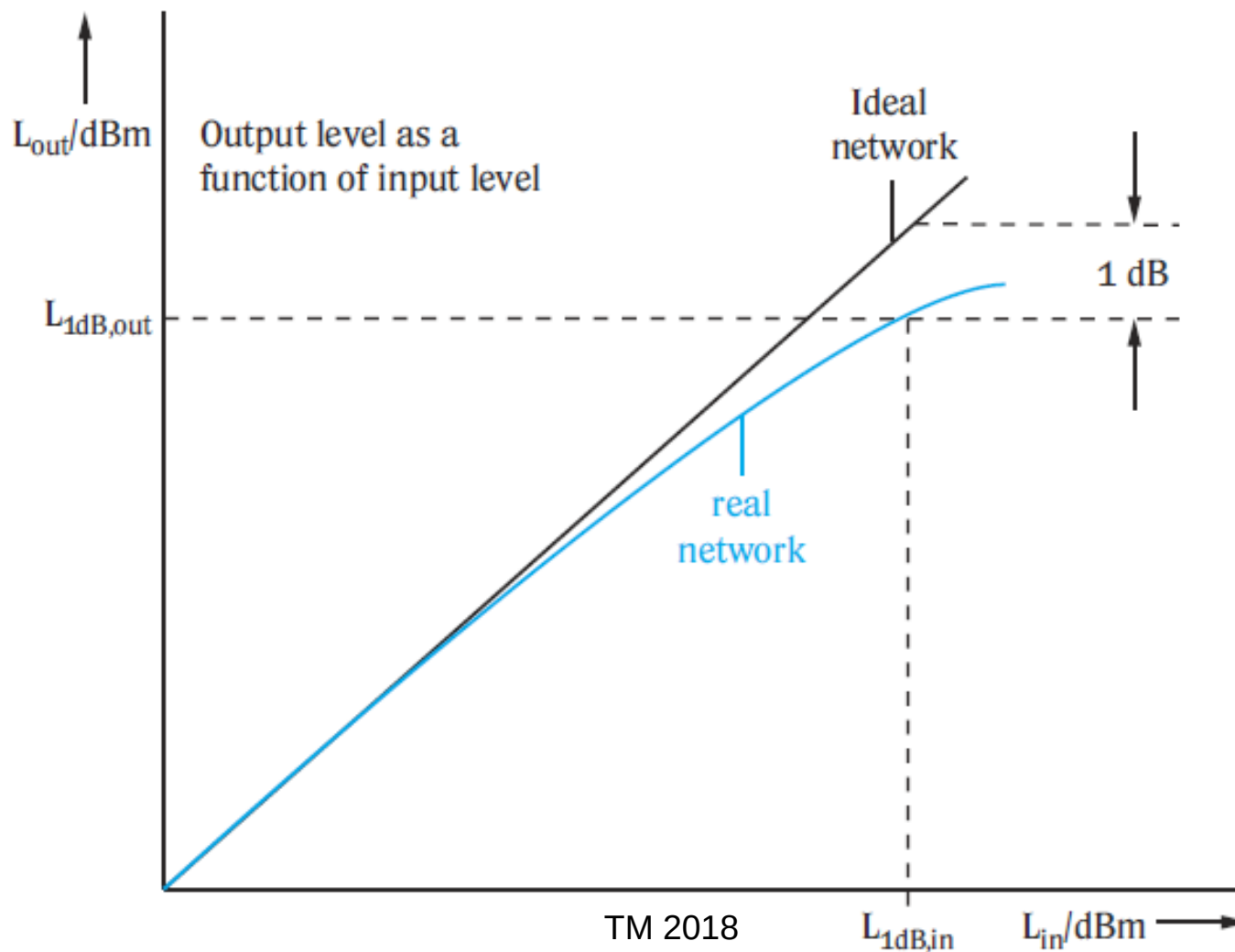
typ. 3 Hz

Typical values for SSB phase noise

Carrier offset	$f_{in} = 500$ MHz	$f_{in} = 3$ GHz	$f_{in} = 7$ GHz
100 Hz	94 dBc/Hz	90 dBc/Hz	84 dBc/Hz
1 kHz	105 dBc/Hz	100 dBc/Hz	94 dBc/Hz
10 kHz	113 dBc/Hz	108 dBc/Hz	104 dBc/Hz
100 kHz	113 dBc/Hz	108 dBc/Hz	106 dBc/Hz
1 MHz	125 dBc/Hz	118 dBc/Hz	118 dBc/Hz

Važi za
span >100 kHz

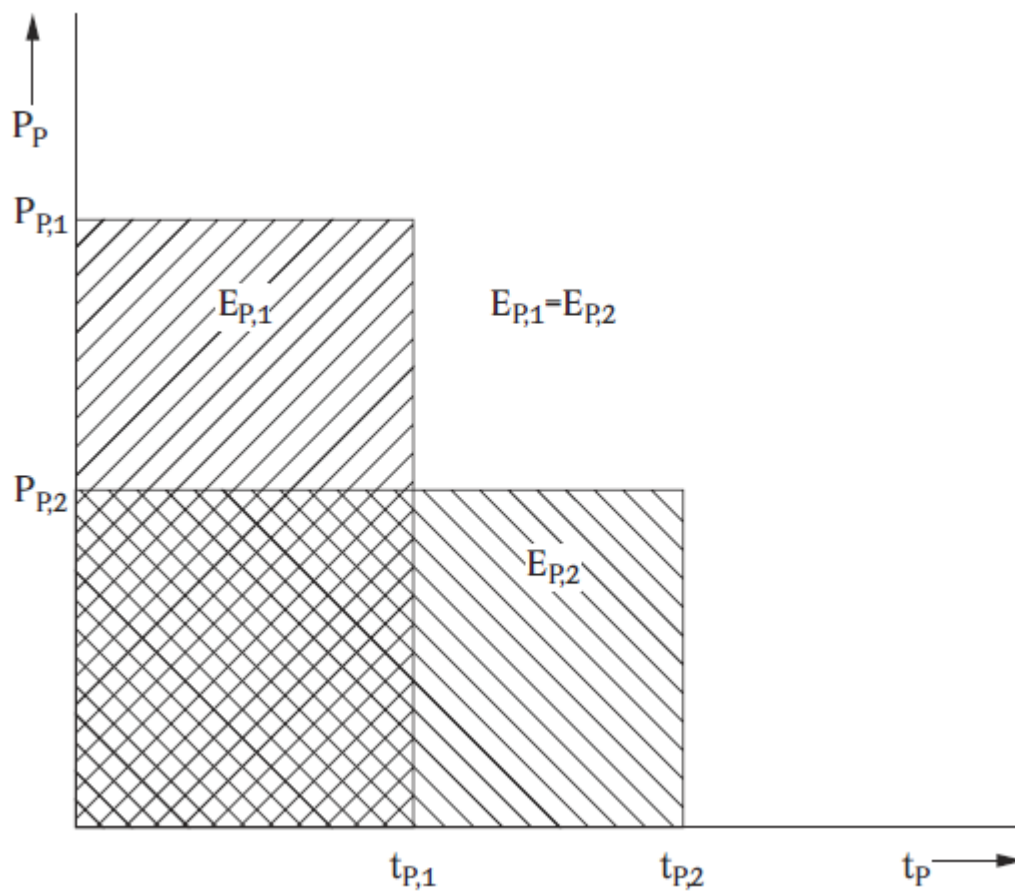
1 dB tačka kompresije



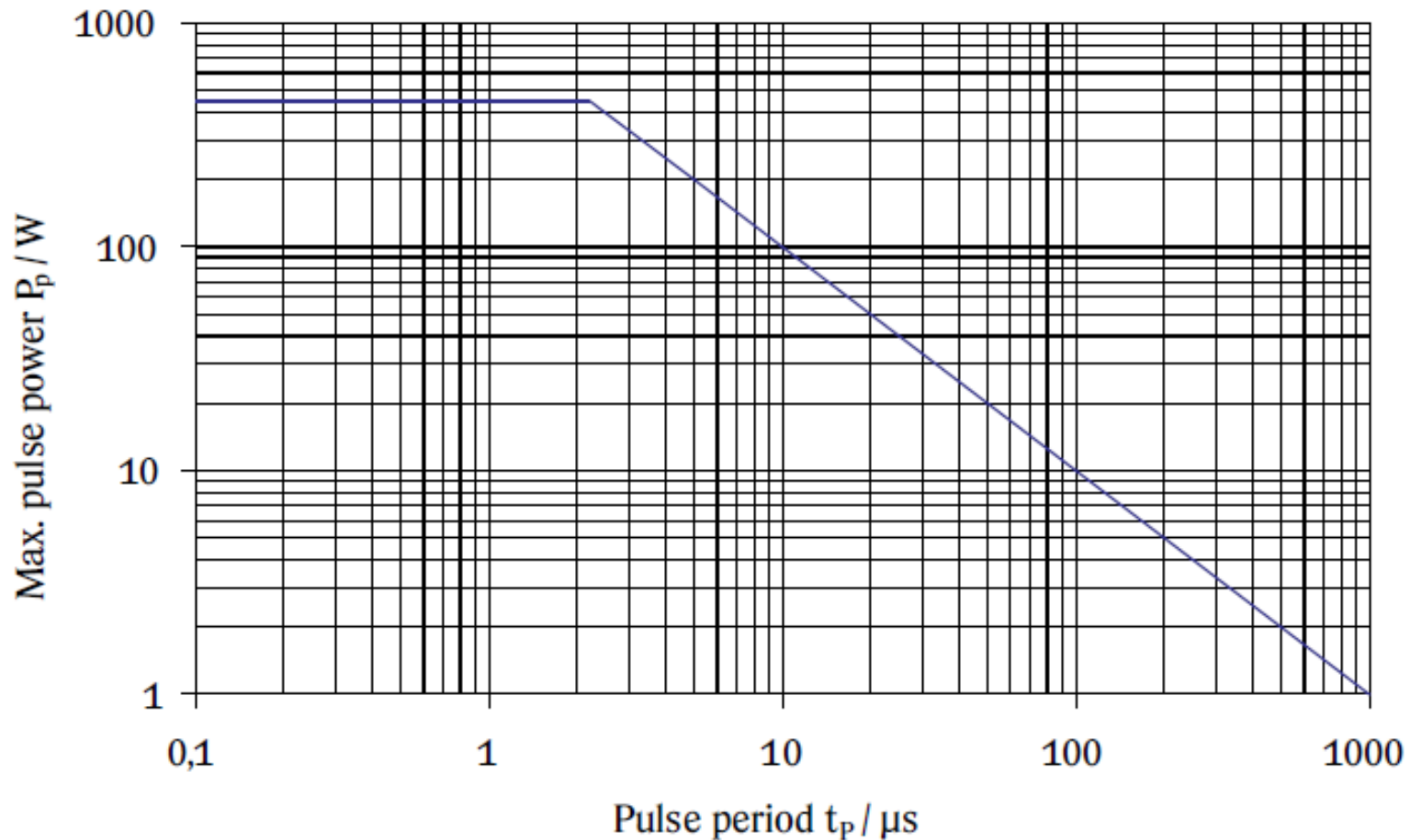
Tipične specifikacije 1 dB tačka kompresije

Maximum input level	
RF attenuation 0 dB	
DC voltage	50 V
CW RF power	20 dBm (= 0.3 W)
Pulse spectral density	97 dB μ V/MHz
RF attenuation 10 dB	
CW RF power	30 dBm (= 1 W)
Max. pulse voltage	150 V
Max. pulse energy (10 μ s)	1 mWs
1 dB compression of output mixer	
0 dB RF attenuation, $f > 200$ MHz	0 dBm nominal

Impulsni signal različite širine a iste energije



Maksimalna snaga Impulsnog signala u funkciji širine



Max. input level

Dinamički opseg

1 dB compression of 1st mixer

Optimum mixer level

Level display range

Max. dynamic range

Max. intermodulation-free range /
max. harmonic suppression

Displayed overrange noise level with selected resolution bandwidth

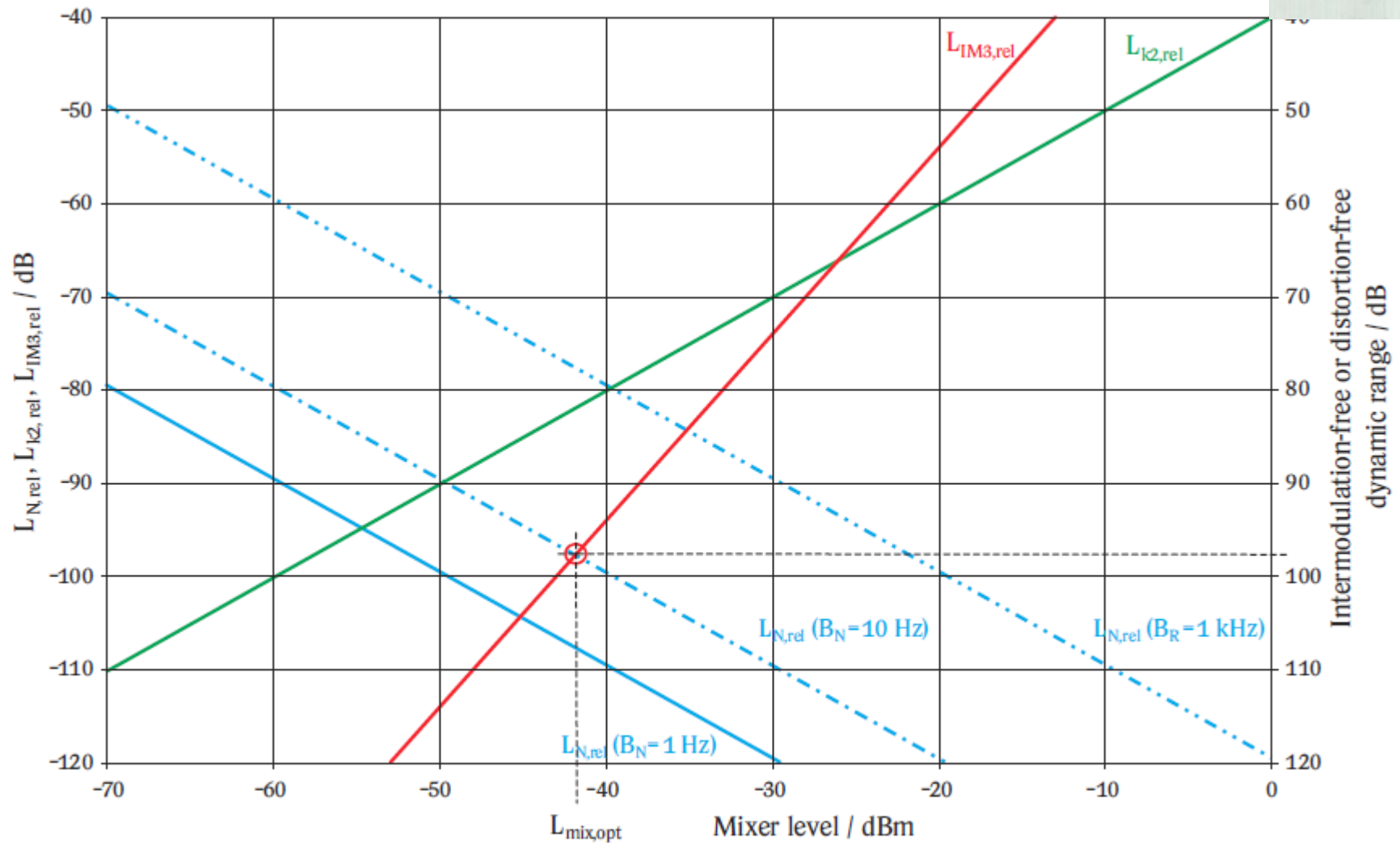


Fig. 5-19 Intermodulation-free range and maximum harmonic suppression as a function of mixer level ($NF = 24.5$ dB, $IP3_{in} = 7$ dBm, $SHI_{in} = 40$ dBm)

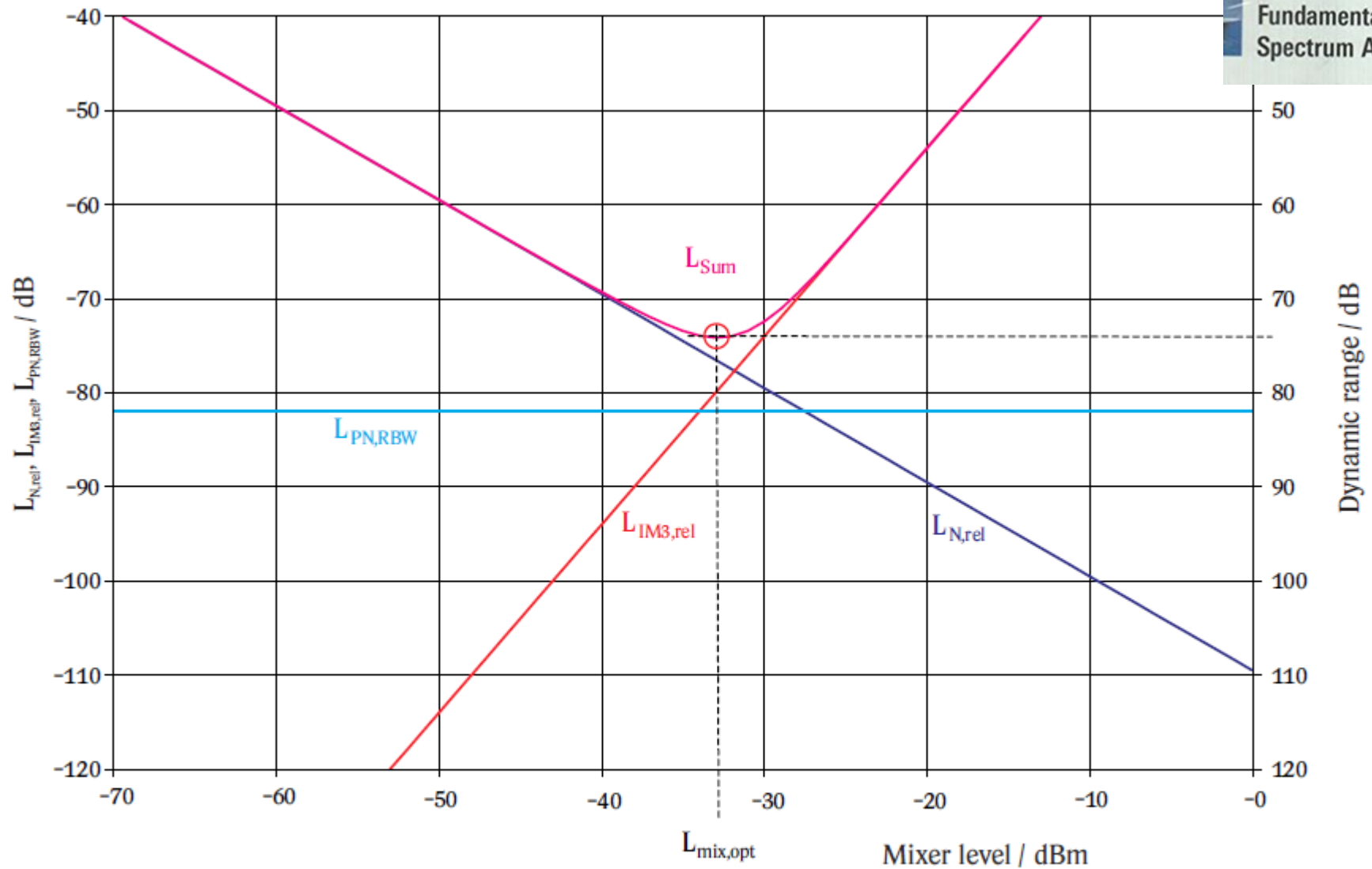


Fig. 5-20 Dynamic range taking into account thermal noise,
phase noise and 3rd order intermodulation products
($NF = 24.5$ dB, $IP3_{in} = 7$ dBm, $L(f_{off}) = -122$ dBc (1Hz), $B_{N,IF} = 10$ kHz)

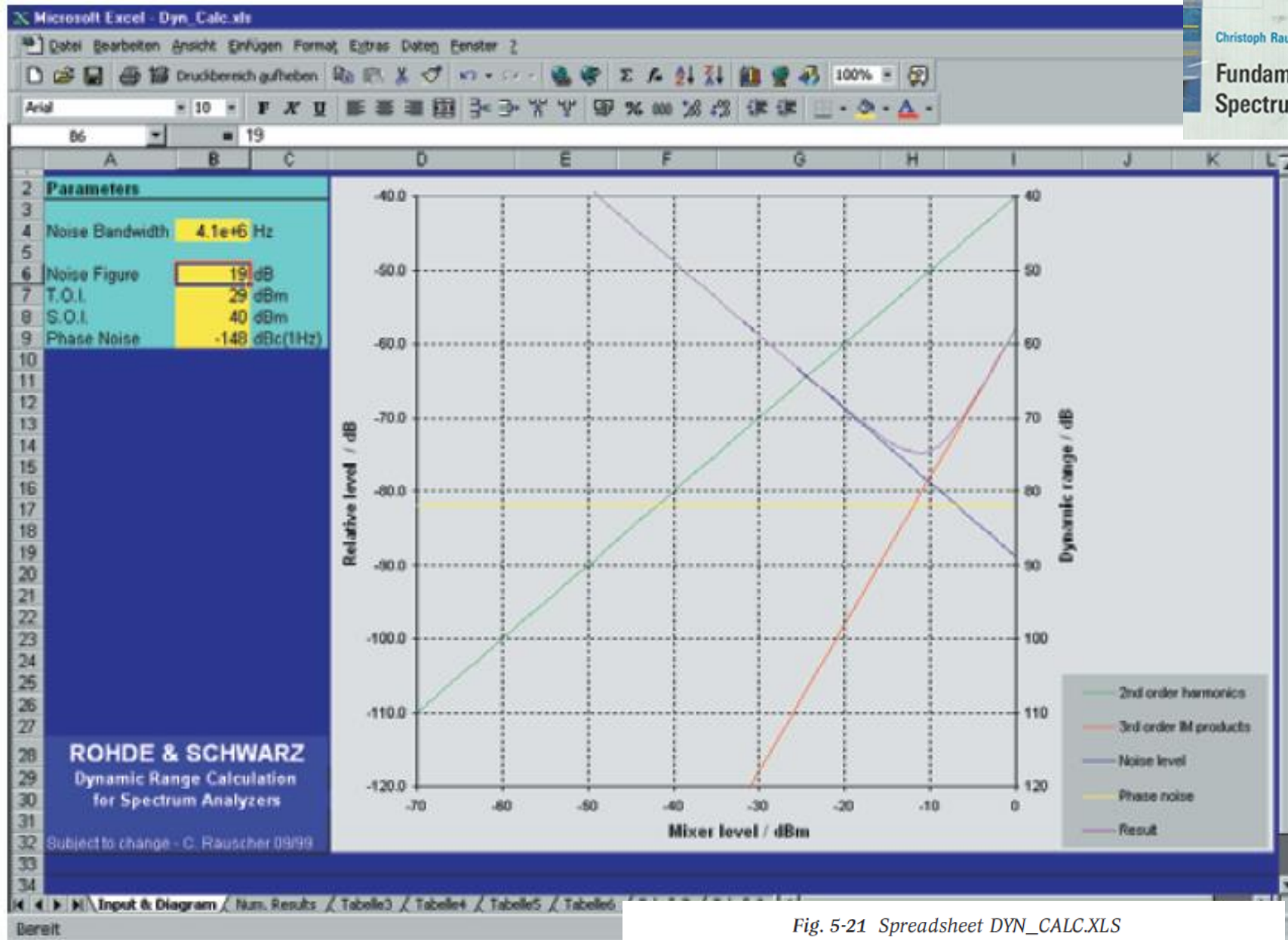


Fig. 5-21 Spreadsheet DYN_CALC.XLS

(a) Input & Diagram sheet: input fields for noise bandwidth, noise figure, TOI, SHI and phase noise as well as graphical representation of resulting dynamic range
 (b) Num. Results sheet: numeric output of results

Microsoft Excel - Dyn_Calc.xls

Datei Bearbeiten Ansicht Einfügen Format Extras Daten Fenster ?

Druckbereich aufheben

Arial 10

B14 = (Input & Diagram!\$B\$8-A14)

	A	B	C	D	E	F	G
		2nd harmonic	Level of 3rd order	Noise floor	Phase noise		
	Mixer level / dBm	(rel. to mixer level) / dB	intermodulation products (rel. to mixer level) / dB	(rel. to mixer level) / dB	contribution / dBc	Result / dB	
1							
2	-70	-110.0	-198.0	-18.9	-81.9	-18.9	
3	-69	-109.0	-196.0	-19.9	-81.9	-19.9	
4	-68	-108.0	-194.0	-20.9	-81.9	-20.9	
5	-67	-107.0	-192.0	-21.9	-81.9	-21.9	
6	-66	-106.0	-190.0	-22.9	-81.9	-22.9	
7	-65	-105.0	-188.0	-23.9	-81.9	-23.9	
8	-64	-104.0	-186.0	-24.9	-81.9	-24.9	
9	-63	-103.0	-184.0	-25.9	-81.9	-25.9	
10	-62	-102.0	-182.0	-26.9	-81.9	-26.9	
11	-61	-101.0	-180.0	-27.9	-81.9	-27.9	
12	-60	-100.0	-178.0	-28.9	-81.9	-28.9	
13	-59	-99.0	-176.0	-29.9	-81.9	-29.9	
14	-58	-98.0	-174.0	-30.9	-81.9	-30.9	
15	-57	-97.0	-172.0	-31.9	-81.9	-31.9	
16	-56	-96.0	-170.0	-32.9	-81.9	-32.9	
17	-55	-95.0	-168.0	-33.9	-81.9	-33.9	
18	-54	-94.0	-166.0	-34.9	-81.9	-34.9	
19	-53	-93.0	-164.0	-35.9	-81.9	-35.9	
20	-52	-92.0	-162.0	-36.9	-81.9	-36.9	
21	-51	-91.0	-160.0	-37.9	-81.9	-37.9	
22	-50	-90.0	-158.0	-38.9	-81.9	-38.9	
23	-49	-89.0	-156.0	-39.9	-81.9	-39.9	
24	-48	-88.0	-154.0	-40.9	-81.9	-40.9	
25	-47	-87.0	-152.0	-41.9	-81.9	-41.9	
26	-46	-86.0	-150.0	-42.9	-81.9	-42.9	
27	-45	-85.0	-148.0	-43.9	-81.9	-43.9	
28	-44	-84.0	-146.0	-44.9	-81.9	-44.9	
29	-43	-83.0	-144.0	-45.9	-81.9	-45.9	
30	-42	-82.0	-142.0	-46.9	-81.9	-46.9	
31	-41	-81.0	-140.0	-47.9	-81.9	-47.9	
32	-40	-80.0	-138.0	-48.9	-81.9	-48.9	

Input & Diagram Num. Results Tabelle3 Tabelle4 Tabelle5 Tabelle6

Bereit

Fig. 5-21 Spreadsheet DYN_CALC.XLS

(a) Input & Diagram sheet: input fields for noise bandwidth, noise figure, TOI, SHI and phase noise as well as graphical representation of resulting dynamic range

(b) Num. Results sheet: numeric output of results

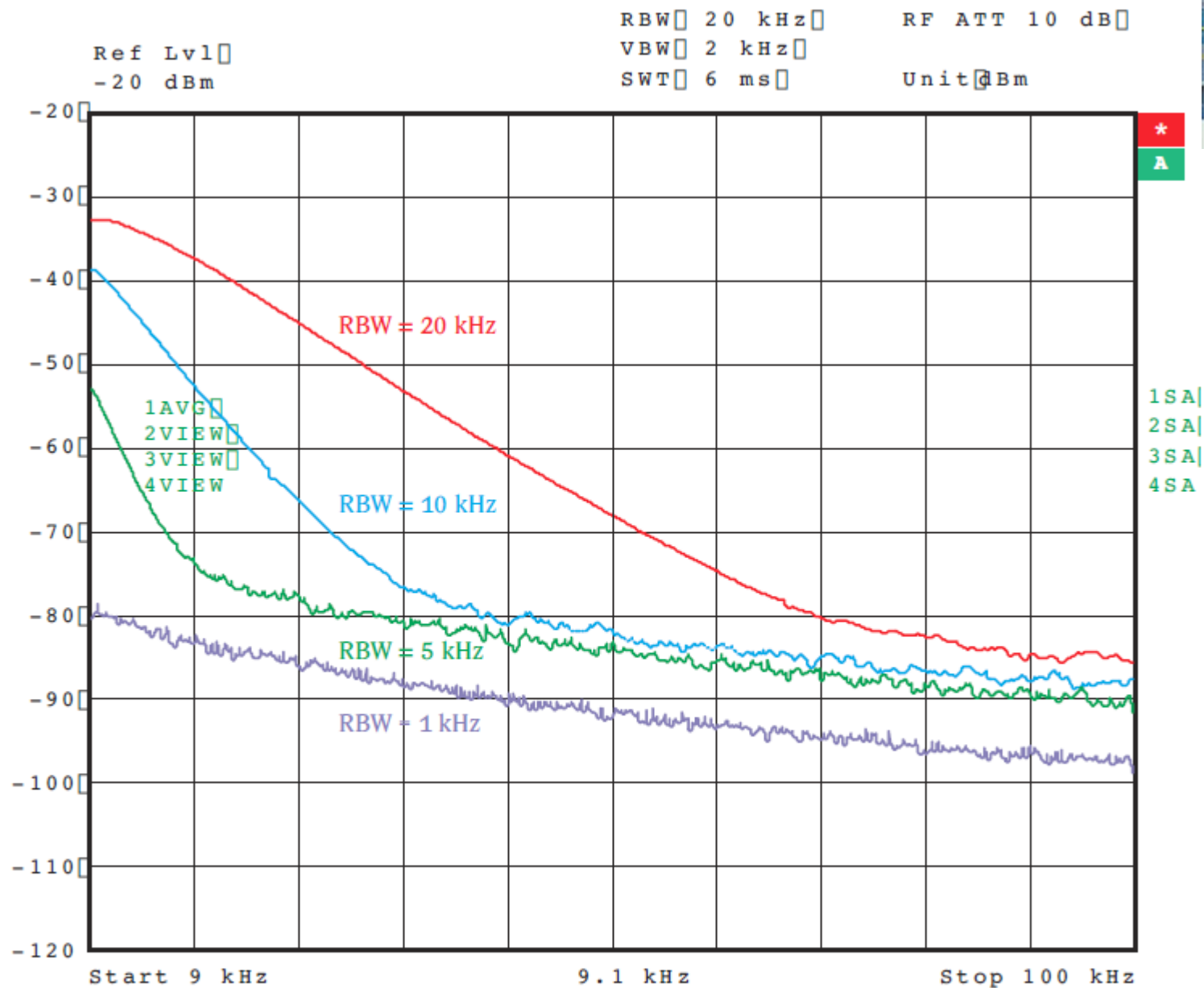


Fig. 5-23 LO feedthrough as a function of selected resolution bandwidth

Improvement of input matching

The RF attenuation of a spectrum analyzer should always be set to at least 10 dB provided that the sensitivity is sufficiently high. In this way the first mixer is protected against damage by too high input signals and the input matching is improved. For example, if an ideal attenuator pad with an attenuation $a = 6$ dB is connected ahead of a twoport with a return loss of $a_r = 10$ dB at the input, the total return loss $a_{r,\text{total}}$ is $a_r + 2 \cdot a$ or 22 dB. Fig. 5-26 shows the spectrum analyzer with the attenuator pad.

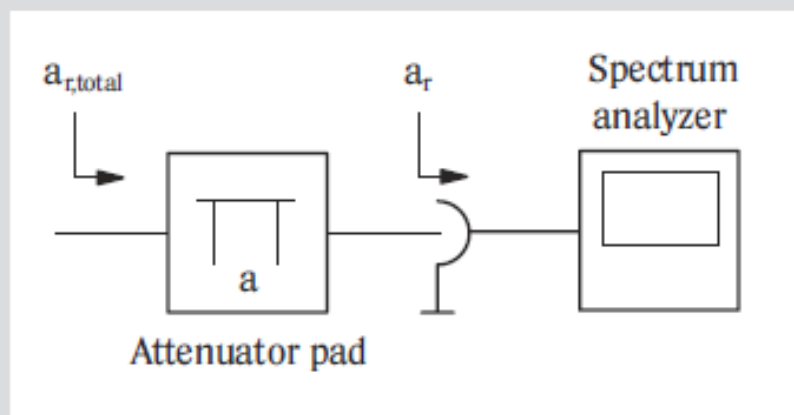


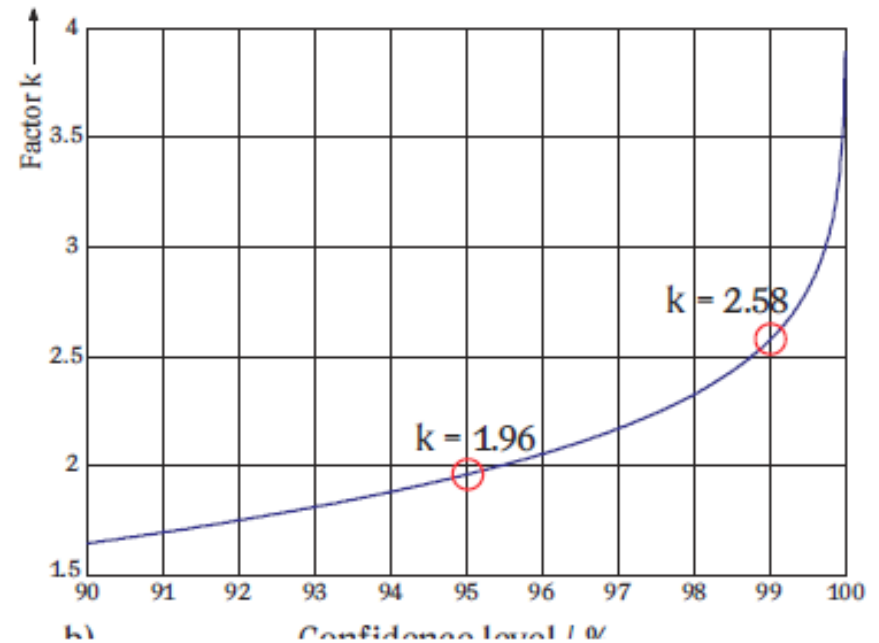
Fig. 5-26 Improvement of spectrum analyzer input matching by connecting an attenuator pad ahead of analyzer

Merna nesigurnost. Doprinos greškama

Measurement Error contribution	Absolute level of CW signal	Harmonic distortion	3rd order intermodulation products (close to carrier)	3rd order intercept	Channel power	Adjacent-channel power ratio	Power versus time (e.g. for TDMA signals), relative	Phase noise, far off carrier, with variation of RF attenuation and reference level	Phase noise, close to carrier
Absolute error	•			•	•				
Frequency response	•	•		•	•				
Attenuator error	•			•	•			•	
IF gain error	•			•	•			•	
Linearity error	•	•	•	•	•	•	•	•	•
Bandwidth switching error	•			•	•				
Bandwidth error					•	•		•	•
Error due to limited number of samples					•	•			
Mismatch error	•	•		•	•				

Table 5-2 Error contributions in typical measurements using a spectrum analyzer

Opseg poverenja

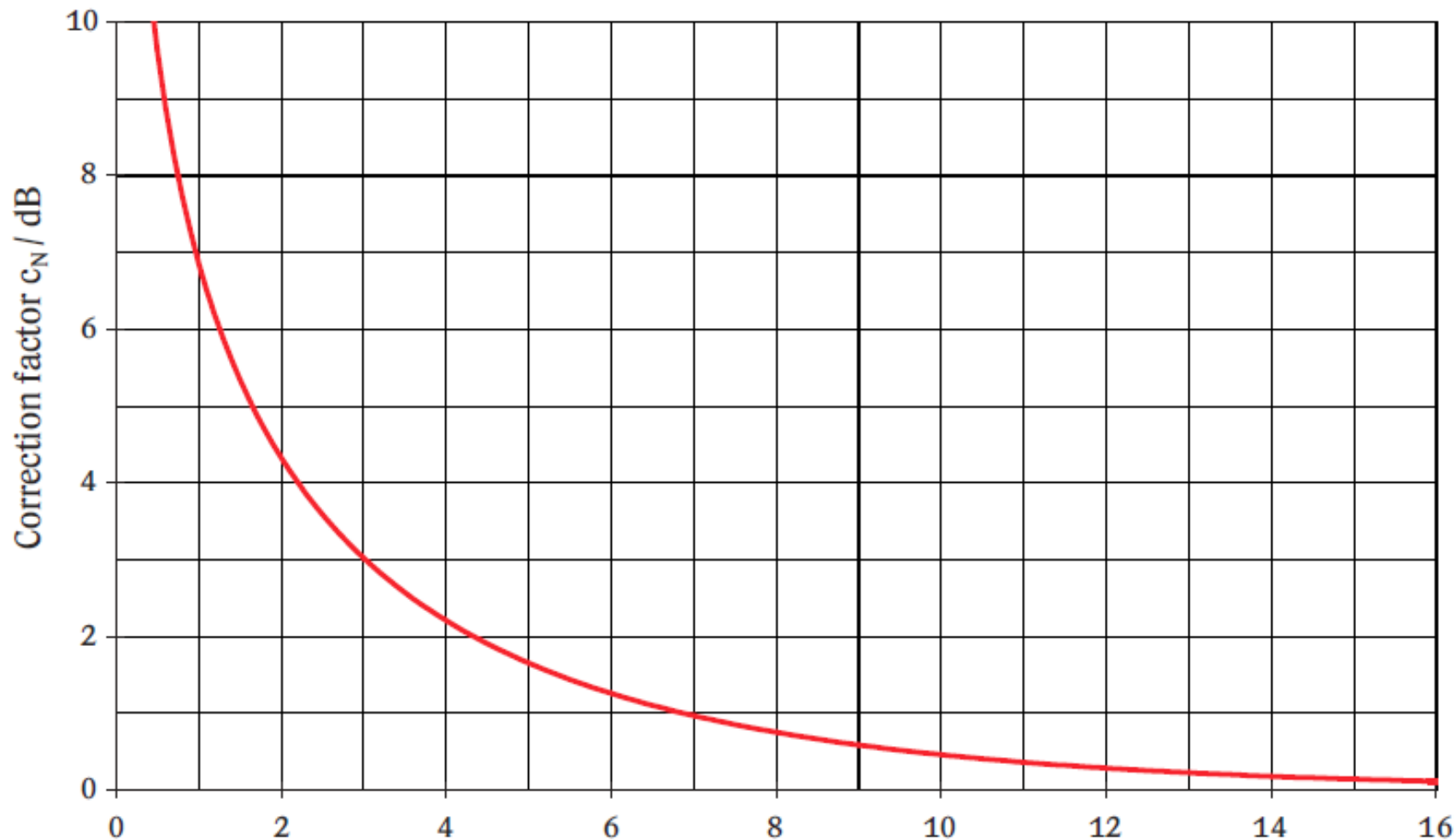


*Fig. 5-27 Coverage factor k as a function of confidence level
a) confidence level 0% to 100%, b) confidence level 90% to 100% (zoomed)*

Error Calculation for Rohde & Schwarz Spectrum Analyzers					
Inherent errors	unit	s = stand. uncertainty w = worst case	specified error	variance σ_i^2	contribute y = yes, n = no
Absolute error 120 MHz	dB	1 w	2 0.3	3 0.03	4 y
Frequency response	dB	w	0.2	0.01	y
Input attenuator	dB	w	0.2	0.01	y
If gain	dB	w	0.2	0.01	y
Log linearity	dB	w	0.2	0.01	y
Bandwidth switching error	dB	w	0.2	0.01	y
Bandwidth error	%		10.00	0.07	y
Combined variance		$\sigma_{\text{tot}}^2 = \sigma_1^2 + \sigma_2^2 + \dots + \sigma_n^2$		0.17	
Combined standard uncertainty		$\sigma_{\text{tot}} = \sqrt{\sigma_{\text{tot}}^2}$		0.41	
Total error (95% confidence level)	dB			0.80	5
(99% confidence level)	dB			1.05	
Error due to source mismatch		a = return loss / dB v = VSWR	specified values		
VSWR of SA		6 v	7 3.1		
VSWR of DUT		v	1.57	0.55	
Combined variance		$\sigma_{\text{tot}}^2 = \sigma_1^2 + \sigma_2^2 + \dots + \sigma_n^2$		0.71	
Combined standard uncertainty		$\sigma_{\text{tot}} = \sqrt{\sigma_{\text{tot}}^2}$		0.85	
Error including source mismatch (95%)	dB			1.66	8
(99%)	dB			2.18	

Fig. 5-28 Spreadsheet FSP_ERR.XLS

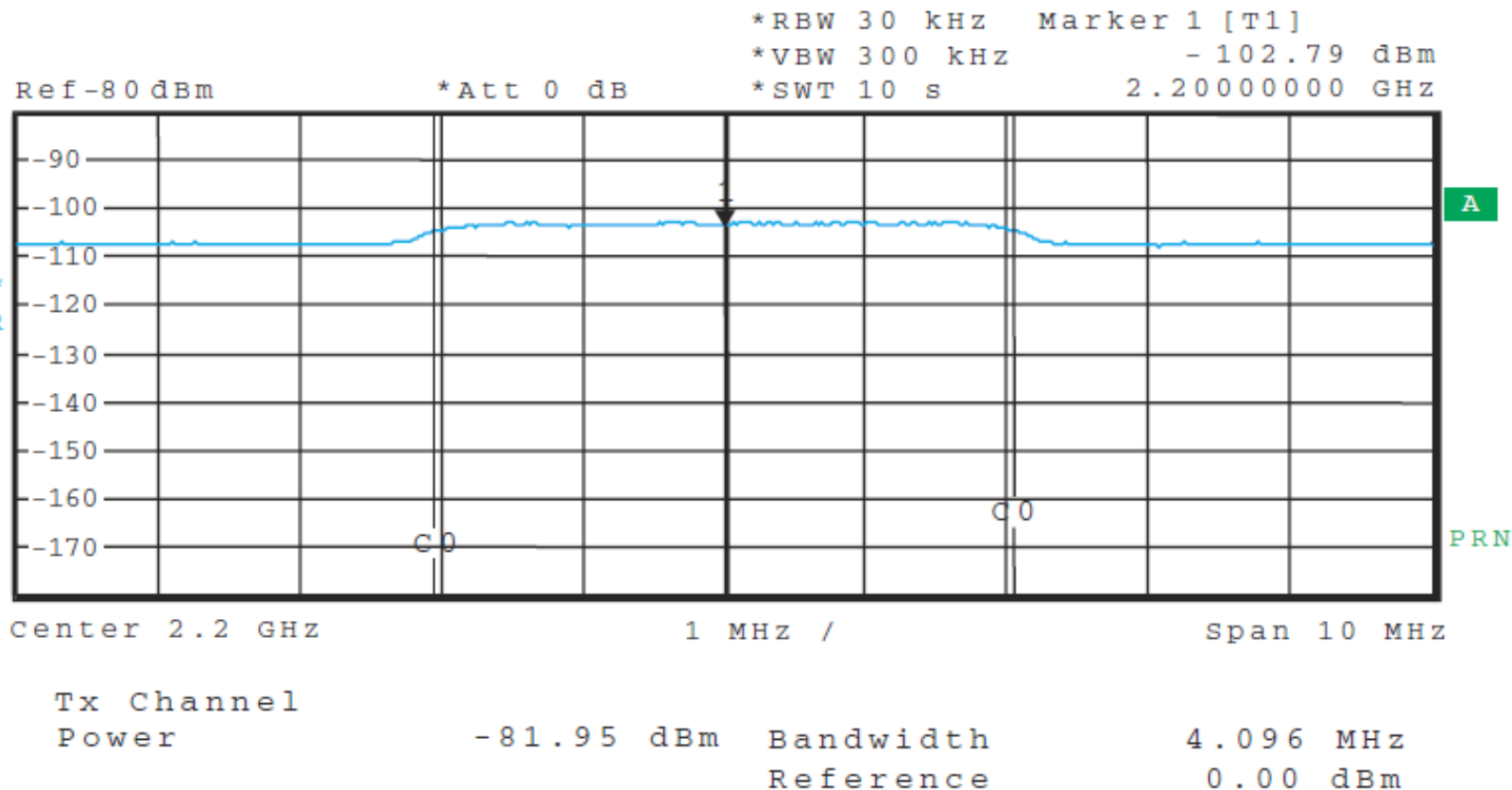
Ukupna snaga / inherentni šum / dB



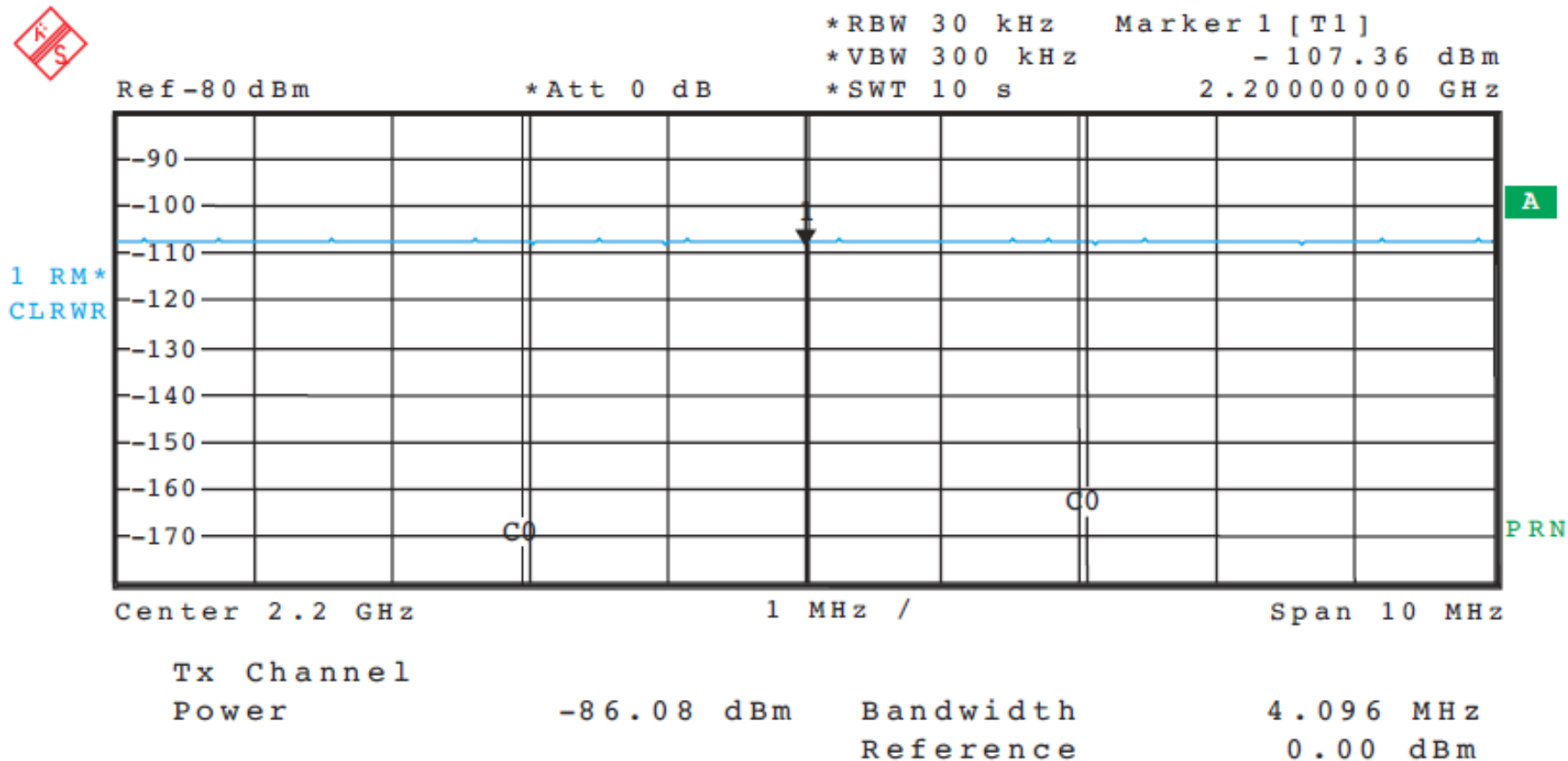
Merenje ukupne snage kanala



1 RM*
CLRWR

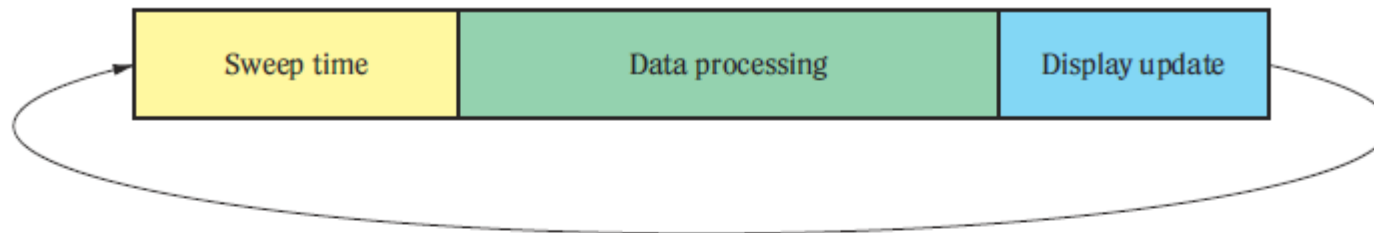


Merenje snage inherentnog šuma



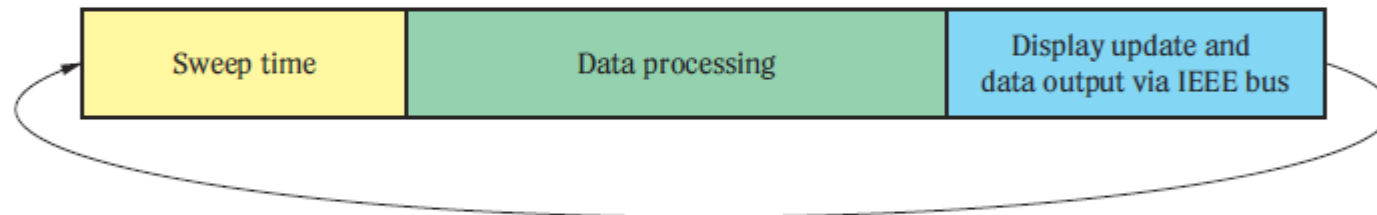
Sekvence merenja

Manual operation

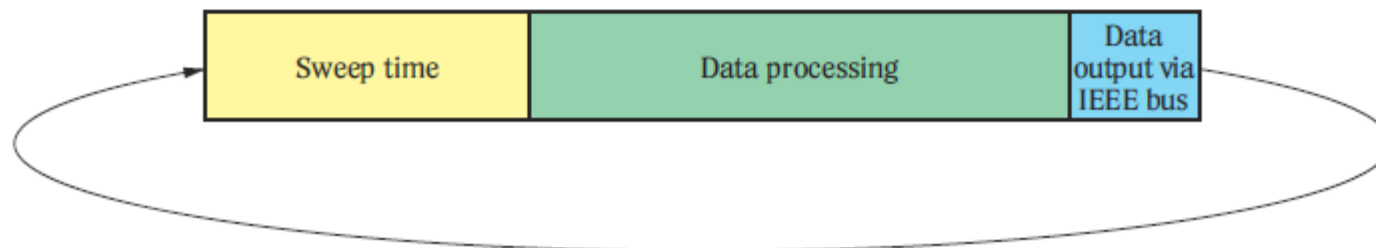


Remote-controlled operation

Display on



Display off



Profesor dr Miroslav Lutovac
mlutovac@viser.edu.rs

Ova prezentacija je nekomercijalna.

Slajdovi mogu da sadrže materijale preuzete sa Interneta, stručne i naučne građe, koji su zaštićeni Zakonom o autorskim i srodnim pravima.

Ova prezentacija se može koristiti samo privremeno tokom usmenog izlaganja nastavnika u cilju informisanja i upućivanja studenata na dalji stručni, istraživački i naučni rad i u druge svrhe se ne sme koristiti –

Član 44 - Dozvoljeno je bez dozvole autora i bez plaćanja autorske naknade za nekomercijalne svrhe nastave:

(1) javno izvođenje ili predstavljanje objavljenih dela u obliku neposrednog poučavanja na nastavi;

- ZAKON O AUTORSKOM I SRODNIM PRAVIMA

("Sl. glasnik RS", br. 104/2009 i 99/2011)