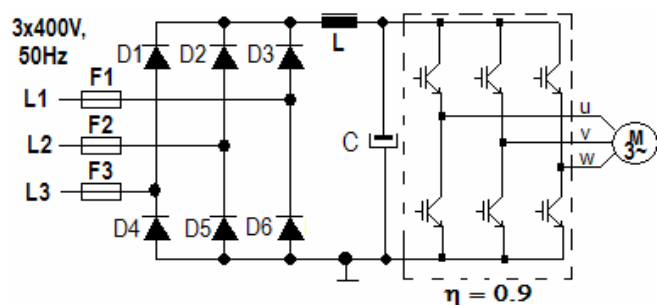


**1. ZADATAK:** Trofazni AC/AC pretvarač na Slici 1 se koristi za frekventnu regulaciju elektromotora čiji su podaci: 400V, 50Hz, 150A, 1485 ob/min,  $\eta = 92\%$ ,  $\cos\varphi = 0.82$ . Stepen iskorišćenja trofaznog tranzistorskog pretvarača je  $\eta_p = 90\%$ . Za ulazni ispravljač su na raspolaganju diodni moduli SKKD100 čiji su tehnički podaci dati u Prilogu 1.



Slika 1- Trofazni AC/AC pretvarač

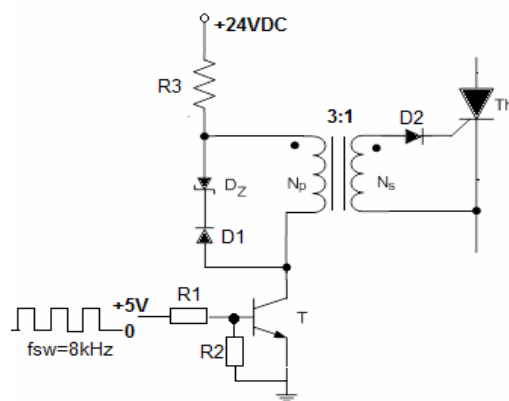
(a) Projektovati LC filter u DC međukolu ako je zahtevana talasnost DC napona  $\leq 1\%$  i talasnost DC struje  $\leq 20\%$ .

(b) Projektovati sistem hlađenja diodnog ispravljača za temperaturni opseg okoline  $-25^\circ\text{C} \dots +40^\circ\text{C}$ , ako se pretpostavi da su svi moduli montirani na istom hladnjaku. Na raspolaganju je hladnjak tipa P3 i ventilator SKF-3-230-1 čiji su tehnički podaci dati u Prilogu 2. Za tako izabrani sistem hlađenja odrediti temperaturu na kućištu modula i temperaturu hladnjaka.

(c) Izvršiti izbor ulaznih osigurača ako su na raspolaganju osigurači dati u Tabeli 1.

Tabela 1

Osigurač	$I^2t$ (A <sup>2</sup> s)	I (A)	AC napon (V)	Vrsta prema brzini
Tip 1	16000	150	690	ultra brzi
Tip 2	15800	150	400	standardni
Tip 3	15500	200	690	ultrabrzi
Tip 4	10000	200	690	standardni
Tip 5	8000	200	440	standardni
Tip 6	30000	250	690	ultrabrzi
Tip 7	62000	315	690	ultrabrzi
Tip 8	2000	125	690	ultrabrzi



Slika 2-Pobudno kolo SCR

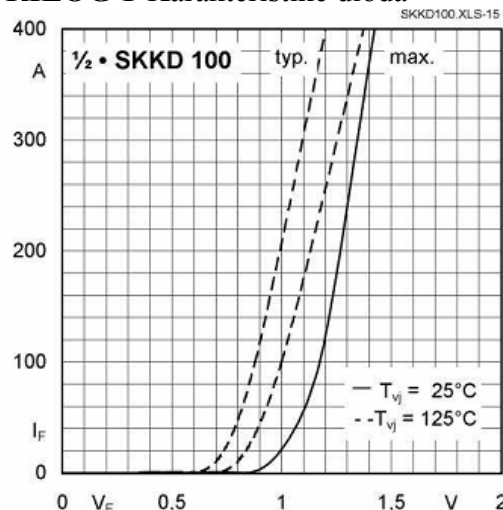
**2. ZADATAK:** Dimenzionisati pobudno kolo tiristora prikazano na Slici 2 ( $R1$ ,  $R2$ ,  $R3$ ,  $V_z$ ), uz pretpostavku da je u kolu gejt tiristora potrebno ostvariti struju od 1.5A pri naponu gejt-katoda od 3V.

Usvojiti da je pad napona na diodama 0.7V, napon  $V_{bes}=0.75V$ , napon  $V_{ces}=0.2V$ , pojačanje tranzistora  $h_{fe}=360$ . Induktivnost magnećenja impulsnog transformatora je 30mH, dok je njegova rasipna induktivnost zanemarljiva.

**3. ZADATAK:** Potrebno je projektovati DC/DC električni neizolovani pretvarač napona koji treba da radi u kontinualnom režimu za koji su dati ulazni podaci za projektovanje: (1) nominalni DC ulazni napon 110V  $\pm 10\%$ , (2) izlazni napon 48VDC, (3) izlazna snaga 1kW, (4) talasnost struje prigušnice  $\leq 10\%$ , (5) talasnost izlaznog napona  $\leq 0.1\%$ , (6) radna učestanost 100kHz. (a) Odrediti kritičnu induktivnost. (b) Dimenzionisati pasivne (L i C) elemente i prekidačke elemente (prema MAX naponu koji moraju izdržati i prema srednjoj vrednosti struje). Zanimariti padove napona i komutacione gubitke na prekidačkim elementima, kao i unutrašnje otpornosti pasivnih elemenata. Smatrati da je opterećenje na izlazu približno konstantno.

**4. ZADATAK:** Potrebno je projektovati DC/DC električni neizolovani pretvarač napona koji treba da radi u kontinualnom režimu, za koji su dati ulazni podaci za projektovanje: (1) nominalni DC ulazni napon 220V  $\pm 10\%$ , (2) izlazni napon 600VDC, (3) izlazna snaga 4kW, (4) talasnost struje prigušnice  $\leq 10\%$ , (5) talasnost izlaznog napona  $\leq 0.1\%$ , (6) radna učestanost 100kHz. (a) Odrediti kritičnu induktivnost. (b) Dimenzionisati prekidačke elemente prema MAX naponu koji moraju izdržati i prema srednjoj vrednosti struje. Zanimariti pad napona na prekidačkom tranzistoru i komutacione gubitke na prekidačkim elementima, kao i unutrašnje otpornosti pasivnih elemenata. Smatrati da je opterećenje na izlazu približno konstantno.

## PRILOG 1-Karakteristike dioda

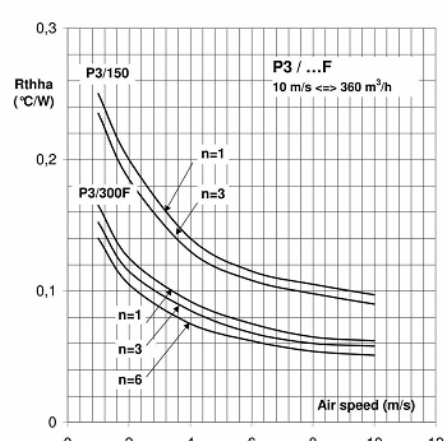
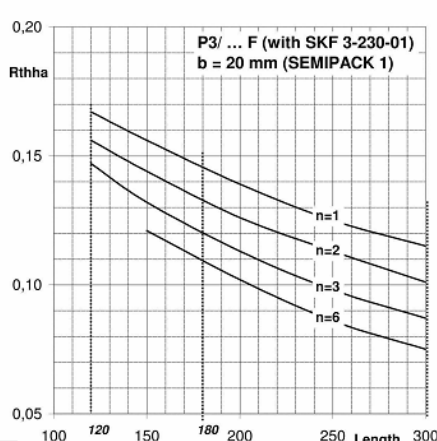
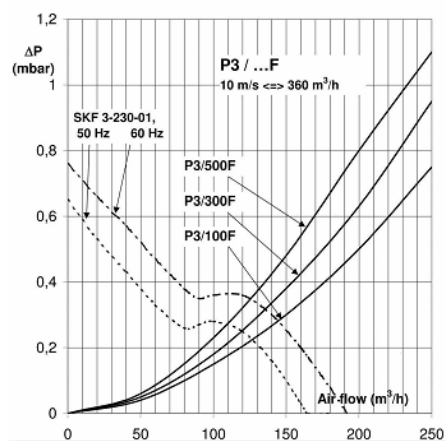
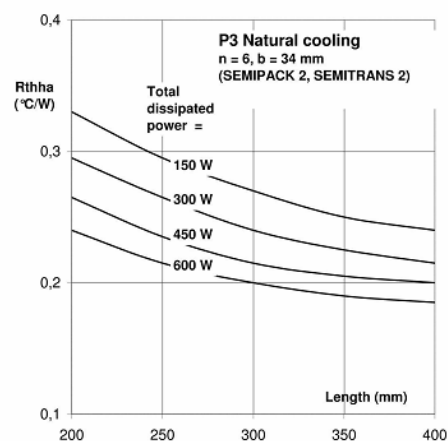
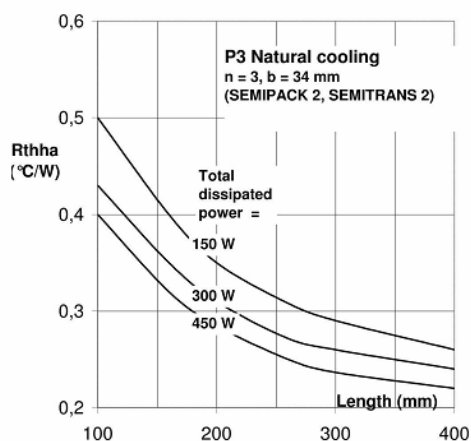
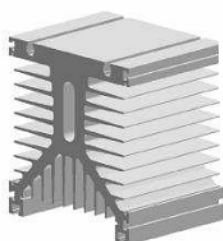


$V_{RSM}$ V	$V_{RRM}$ V	$I_{FRMS} = 175 \text{ A}$ (maximum value for continuous operation) $I_{FAV} = 100 \text{ A}$ (sin. 180; $T_c = 85^\circ\text{C}$ )	
500	400	SKKD 100/04	
900	800	SKKD 100/08	
1300	1200	SKKD 100/12	
1500	1400	SKKD 100/14	
1700	1600	SKKD 100/16	
1900	1800	SKKD 100/18	

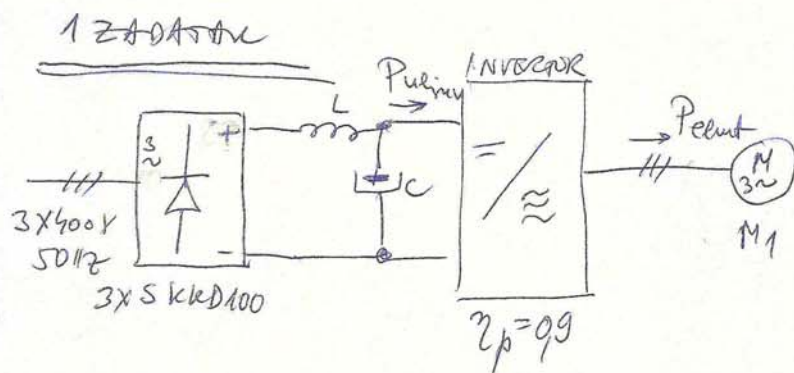
Symbol	Conditions	Values	Units
$I_{FAV}$	sin. 180; $T_c = 85$ (100) $^\circ\text{C}$	100 (67)	A
$I_D$	P3/180; $T_a = 45^\circ\text{C}$ ; B2 / B6	73 / 91	A
	P3/180F; $T_a = 35^\circ\text{C}$ ; B2 / B6	150 / 190	A
$I_{FSM}$	$T_{vj} = 25^\circ\text{C}$ ; 10 ms	2500	A
	$T_{vj} = 125^\circ\text{C}$ ; 10 ms	2000	A
$i^2t$	$T_{vj} = 25^\circ\text{C}$ ; 8,3 ... 10 ms	31250	A <sup>2</sup> s
	$T_{vj} = 125^\circ\text{C}$ ; 8,3 ... 10 ms	20000	A <sup>2</sup> s
$R_{th(j-c)}$	per diode / per module	0,35 / 0,175	K/W
$R_{th(c-s)}$	per diode / per module	0,2 / 0,1	K/W
$T_{vj}$		- 40 ... + 125	$^\circ\text{C}$
$T_{slg}$		- 40 ... + 125	$^\circ\text{C}$

## PRILOG 2- Karakteristike hladnjaka i ventilatora

Standard lengths	n	b / d Ø mm	$R_{thha}$ natural cooling K/W	$R_{thha}$ with Fan SKF 3-230-01 K/W	w kg
P 3/120	1	20	0,55 (100W)	0,167	2,1
	3		0,43 (150W)	0,147	
P 3/180	2	20	0,39 (150W)	0,132	3,1
	3		0,36 (180W)	0,12	
	6		0,33 (200W)	0,108	
	1	34		0,144	
	3			0,118	
P 3/300	3	34		0,0847	5,3



1



M1:

$$U_n = 400V$$

$$f_n = 50Hz$$

$$I_n = 150A$$

$$\eta_n = 14.85\%$$

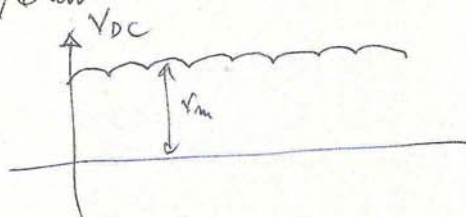
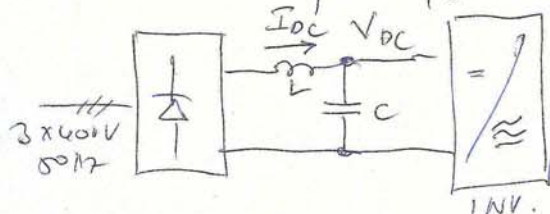
$$z_n = 92\%$$

$$\cos \phi_n = 0.92$$

$$P_{elout} = \sqrt{3} U_n I_n \cos \phi_n = \sqrt{3} \cdot 400 \cdot 150 \cdot 0.92 = 85.1 kW$$

$$P_{mot} = z_n \cdot P_{elout} = 78.1 kW$$

$$P_{elinv} = \frac{P_{elout}}{z_p} = \frac{85.1}{0.9} = 94.6 kW$$



$$V_{DC} = \frac{3 V_m}{\pi}$$

$$V_{DC} = \frac{3 \cdot \sqrt{2} \cdot 400V}{\pi}$$

$$V_{DC} = 538.85V$$

Ано се узму и обзир падови напон на диодима и испрежен  $V_D = 2 \times V_{D1} =$

$$V_D = 2 \times 1.2V \approx 2.4V \Rightarrow V_{DC}^* = \frac{3(\sqrt{2} \cdot 400 - 2 \cdot 1.2V)}{\pi} = \frac{3 \cdot 561.6}{\pi} = 536.56V$$

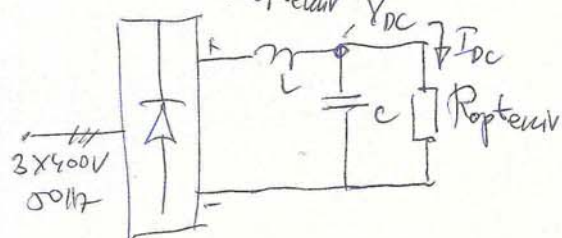
$$I_{DC} = \frac{V_{DC}^*}{R_{optenr}} \Rightarrow \frac{536.56V}{1763A} = R_{optenr}$$

$$P_{DC} = P_{elinv} = 94.6 kW$$

$$P_{DC} = (V_{DC}^*) \cdot I_{DC} \Rightarrow I_{DC} = \frac{P_{DC}}{V_{DC}^*} = \frac{94.6 kW}{536.56V}$$

$$I_{DC} = 176.3A$$

$$R_{optenr} = \frac{536.56}{176.3} = 3.043 \Omega$$



$$U_{ispr} = V_{DC}^* + \frac{6 V_m \cos 6\omega t}{35} - \frac{6 V_m \cos 12\omega t}{143\pi} - \dots$$

$$U_{ispr} \approx V_{DC}^* + \frac{6 V_m \cos 6\omega t}{35\pi}$$

$$U_{ispr}^{(6)} = 30.66V$$

$$V_{DC}^* = 536.56V$$

$$U_{ispr}^{(6)} = \frac{6 V_m}{35\pi} = \frac{6 \cdot (\sqrt{2} \cdot 400V - 2.4V)}{35\pi}$$

$$U_{ispr}^{(6)} = 30.66V$$

(2)

a) \* izbor kondenzatora C u "LC" Filteru

$$C \geq \frac{1}{\eta \cdot \omega \cdot R_{\text{ortekv}}} \cdot \frac{\delta_i}{\delta_n}$$

 $\eta = 6$  (feritni materijal)

$$\omega = 2\pi f = 2\pi \cdot 50 \text{ Hz} = 314 \text{ rad/s}$$

$$C \geq \frac{1}{6 \cdot 314 \cdot 3,043} \cdot \frac{20}{1}$$

$$R_{\text{ortekv}} = 3,043 \Omega$$

$$\delta_{i\%} = 20\% \rightarrow \delta_i = 0,2$$

$$\delta_{n\%} = 1\% \rightarrow \delta_n = 0,01$$

$$C \geq 3488,56 \mu\text{F}$$

$$\text{Maksimalna se } C^* = 3600 \mu\text{F} / 800 \text{ V}_{\text{DC}}$$

$$\text{kritična induktivnost: } L_{\text{kr}} = \frac{R_{\text{ortekv}}}{105 \omega} = \frac{3,043}{105 \cdot 314} = 92,3 \mu\text{H}$$

\* izbor induktivnog Filtera

$$L \gg L_{\text{kr}}$$

$$\frac{\Delta I_L^{(6)}}{I_{\text{DC}}} = \frac{4 R_{\text{ortekv}}}{35} \cdot \frac{6 \omega C^*}{(6 \omega)^2 L C^* - 1} \leq 0,2 \quad \text{odavde}$$

$$L \geq \frac{1}{(6 \omega)^2 C^*} \cdot \frac{4 R_{\text{ortekv}} \cdot 6 \omega C^*}{35 \cdot 0,2} + \frac{1}{(6 \omega)^2 C^*}$$

$$L \geq \frac{4 R_{\text{ortekv}}}{35} \cdot \frac{1}{6 \omega} \cdot \frac{1}{0,2} + \frac{1}{(6 \omega)^2 \cdot C^*}$$

$$L \geq \frac{4 \cdot 3,043}{35} \cdot \frac{1}{6 \cdot 314} \cdot \frac{1}{0,2} + \frac{1}{(6 \cdot 314)^2 \cdot 36 \cdot 10^{-3}}$$

$$L \geq 0,0009224 + 0,000078259$$

$$L \geq 0,922 \text{ mH} + 0,078 \text{ mH} \approx 1 \text{ mH} \rightarrow \text{Maksimalna se } L^* = 1 \text{ mH}$$

$$I_{\text{DC}} = 176,3 \text{ A}$$

$$\Delta I_{\text{DC}} = 0,2 \cdot 176,3 = 35,26 \text{ A}$$

$$I_{\text{Lmax}} = I_{\text{DC}} + \frac{\Delta I_{\text{DC}}}{2} = 176,3 \text{ A} + 17,63 = 194 \text{ A} \rightarrow 200 \text{ A}$$

$$L^* = 1 \text{ mH} / 200 \text{ A}$$

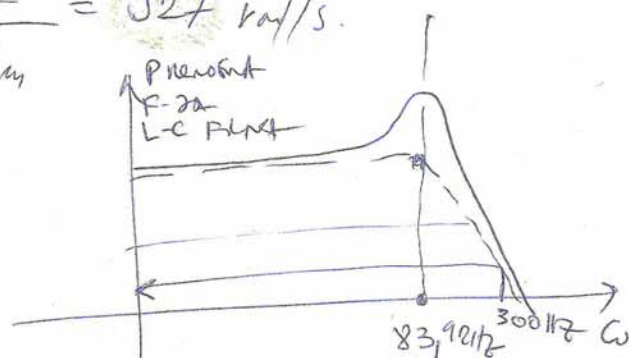


rezonantna mreža „LC“ Filter

(3)

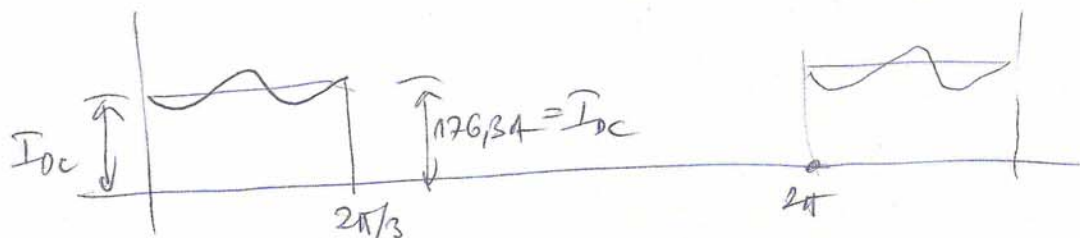
$$\omega_{rez} = \frac{1}{\sqrt{L^* \cdot C^*}} = \frac{1}{\sqrt{1\mu \cdot 36\mu}} = 527 \text{ rad/s.}$$

$$f_{rez} = \frac{\omega_{rez}}{2\pi} = \frac{527}{6,28} = 83,92 \text{ Hz}$$



Filter propuske niskih  
frekvencija

b) Transformator snage diode  
u 1 faznom



snaga mrežne snage diode:

$$I_{DR} = \frac{I_{DC}}{2\pi} \cdot \frac{2\pi}{3} = \frac{I_{DC}}{3} = \frac{176,3}{3} = 58,76 \text{ A}$$

efektivna mrežna snaga diode:

$$I_{Deff} = \sqrt{\frac{1}{2\pi} \int_0^{2\pi} I_{DC}^2 \cdot \frac{2\pi}{3}} = \frac{I_{DC}}{\sqrt{3}} = \frac{176,3}{\sqrt{3}} = 102 \text{ A}$$

disipacija na čvoru diode:

$$P_{D1} = V_{T0} \cdot I_{DR} + r_d \cdot I_{Deff}^2$$

$r_d$  - otpor diode

SA GRAFIKOM I-V KARAKTERISTIKA (PRILOG 1) ZA KARAKTERISTIKU  
MAX i PR MAX temp.  $T_j = +125^\circ\text{C}$  je očigledno da je

$$V_{T0} = 1 \text{ V} \quad r_d = \frac{1,4 - 1}{400 - 0} = 1 \text{ m}\Omega$$

$$P_{D1} = 1 \cdot 58,76 + 1\text{m} \cdot 102^2 = 58,76 \text{ W} + 10,4 \text{ W} = 69,16 \text{ W} \approx 70 \text{ W}$$

UKUPNA DISIPACIJA SVA 6 DIODA

$$\Sigma P_D = 6 \cdot 70 \text{ W} = 420 \text{ W}$$

$$T_{j\max} = +125^{\circ}\text{C}$$

$$T_{\text{amb}} = +40^{\circ}\text{C} \text{ (MAX REP. OKOLNE)}$$

J - JUNCTION (dvoj)  
C - case (kućiste)  
S - sink (hlavina)

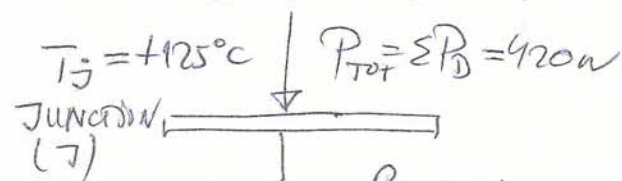
(4)

iz prikaza - 1 za termične otpornosti kućista dijela te doraba

$$R_{th(j-c)}_1 = 0,35 \frac{\text{K}}{\text{W}} \text{ (za jedan dio odn)} - \text{term. otp. J-C}$$

$$R_{th(c-s)}_1 = 0,2 \frac{\text{K}}{\text{W}} \text{ (za jedan dio odn)} - \text{term. otpor. C-S}$$

Eniv. termički Jct:



$$\Sigma R_{th} = R_{th(j-c)} + R_{th(c-s)} + R_{th(s-a)}$$

$$\frac{R_{th(j-c)}_1}{6} = \frac{0,35}{6} = 0,0583 \frac{\text{K}}{\text{W}} = R_{th(j-c)}_e$$

$$\frac{R_{th(c-s)}_1}{6} = \frac{0,2}{6} = 0,0333 \frac{\text{K}}{\text{W}} = R_{th(c-s)}_e$$

$$R_{th(s-a)} = ?$$

$$\Sigma R_{th} \leq \frac{T_{j\max} - T_{\text{amb}}}{P_{\text{tot}}}$$

$$\Sigma R_{th} \leq \frac{125 - 40}{420} = 0,2 \frac{\text{K}}{\text{W}}$$

$$R_{th(j-c)}_e + R_{th(c-s)}_e + R_{th(s-a)} \leq 0,2 \frac{\text{K}}{\text{W}}$$

$$R_{th(s-a)} \leq 0,2 - 0,0583 - 0,0333 = 0,1084 \frac{\text{K}}{\text{W}}$$

$$* R_{th(s-a)} \leq 0,1 \frac{\text{K}}{\text{W}}$$

Primjerice se forsirano hladjenje i mjenjač se hladio P3/300F i za mjenjači ventilatorne SUF 3-230-01/5012

te doraba, RAONI protok vazduha od  $120 \frac{\text{m}^3}{\text{h}} \rightarrow 3,3 \frac{\text{m}^3}{\text{s}}$

za  $n=3$  (3 mjenjača) i za  $3,3 \frac{\text{m}^3}{\text{s}}$  za P3/300F se doraba

$$R_{th(s-a)} = 0,09 \frac{\text{K}}{\text{W}} \leq 0,1 \frac{\text{K}}{\text{W}}$$

5

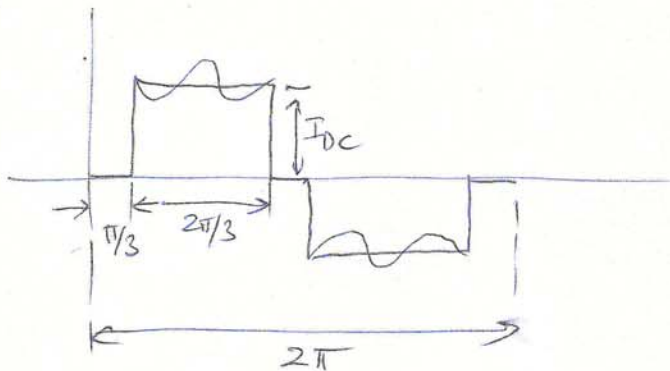
temperatura hladnjača

$$T_s = T_{amb} + R_{th(s-a)} \cdot P_{TOT} = 40^\circ\text{C} + 9,09 \frac{\text{K}}{\text{W}} \cdot 420\text{W} = 77,8^\circ\text{C}$$

temperatura kućnog

$$T_c = T_s + R_{th(c-s)} \cdot P_{TOT} = 77,8^\circ\text{C} + 9,033 \cdot 420 = 91,8^\circ\text{C}$$

c) Efektivna vrednost linijne struje.



$$I_{Leff} = \sqrt{\frac{2 \cdot I_{DC}^2 \cdot \frac{2\pi}{3}}{2\pi}}$$

$$I_{Leff} = \sqrt{\frac{2}{3}} I_{DC}$$

$$I_{Leff} = 0,8164 \cdot 176,3\text{A} = 144\text{A}$$

uslovat se osigurač za 150A (ultra-brzi)

UBO - ultra brz o sigurno

$$I^2 \cdot t_{(Diode)} > I^2 \cdot t_{(UBO)}$$

pretpostavka

$$I^2 \cdot t_{(Diode)} \approx 2 I^2 \cdot t_{(UBO)} \Rightarrow I^2 \cdot t_{(UBO)} = \frac{1}{2} \cdot I^2 \cdot t_{(Diode)}$$

$$I^2 \cdot t_{(UBO)} = \frac{1}{2} \cdot \underbrace{20000 \text{ A}^2 \cdot \text{s}}_{\text{podatak iz tabele za diodu (PR106-1) pri } +125^\circ\text{C}} \approx 10000 \text{ A}^2/\text{s} < 16000 \text{ A}^2/\text{s}?$$

podatak iz tabele za diodu (PR106-1) pri +125°C

uslovat se ultra brzi osigurač TIP 1: 150A/16000 A²s/690V~







Usrednja je  $V_Z^* = 11V$

(7)

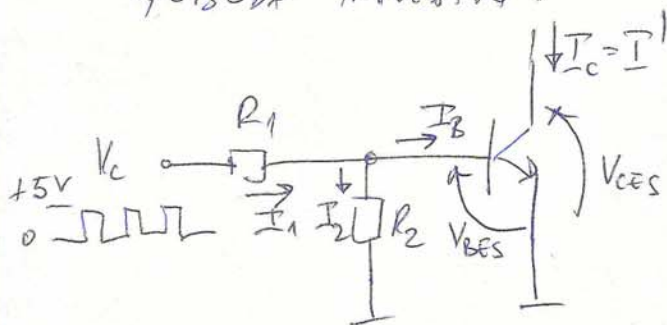
$$t_{off}^* = \frac{L_m \cdot \Delta i'}{V_Z^* + V_D} = \frac{30 \mu H \cdot 23,1 \mu A}{11 + 0,7} = 59,2 \mu s < 62,5 \mu s \quad \checkmark$$

Disipacija na Zener diodi

$$P_D = V_Z \cdot \Delta i' \cdot \frac{t_{off}}{T} = 11 \cdot 23,1 \mu A \cdot \frac{59,2 \mu}{125 \mu} = 0,12 W$$

$$V_Z^* = 11V / 0,25W$$

POBUDA KONTAKTA:



$$I_1 = I_2 + I_B$$

$$I_1 = \frac{V_C - V_{BES}}{R_1} \quad I_B \geq \frac{I_C}{h_{FE}} = \frac{I'}{h_{FE}}$$

$$I_2 = \frac{V_{BES}}{R_2}$$

$$I_B \geq \frac{0,5}{360}$$

$$I_B \geq 1,388 \mu A$$

$R_2 \gg R_1$  i usrednjeno  $R_2 = 10k$ .

$$I_2 = \frac{V_{BES}}{R_2} = \frac{0,75}{10k} = 0,075 \mu A$$

$$I_B^* = 2 \mu A$$

$$I_1 = I_2 + I_B$$

$$I_B^* = I_1 - I_2 = 2 \mu A$$

$$I_1 = 2 \mu A + 0,075 \mu A = 2,075 \mu A$$

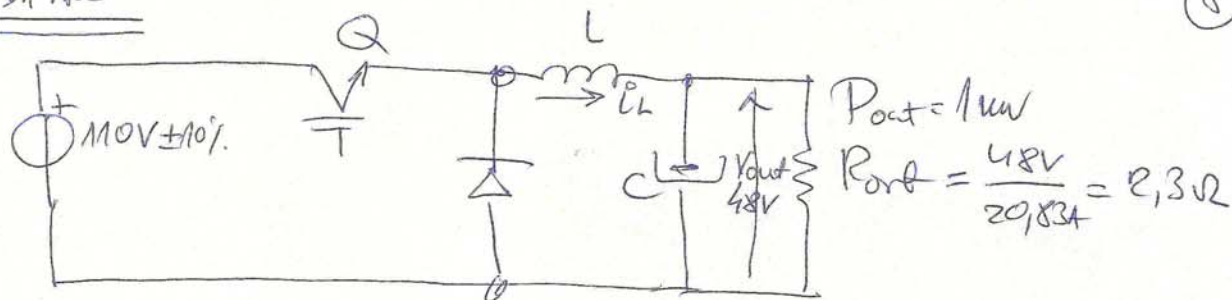
$$R_1 = \frac{V_C - V_{BES}}{I_1} = \frac{5 - 0,75}{2,075} \cdot 10^3 = 2k\Omega$$

$$P_{R1} = R_1 \cdot I_{R1,eff}^2 = 2k \cdot 2,075 \mu^2 = 8,6 \mu W$$

$$\begin{array}{l} R_1^* = 2k; 1/4W \\ R_2^* = 10k 1/4W \end{array}$$

3 zadane

8



$$\Delta i_L \leq 10\%$$

$$f_{sw} = 100 \text{ kHz}$$

$$I_{out} = \frac{P_{out}}{V_{out}} = \frac{100 \text{ W}}{48 \text{ V}}$$

$$\Delta V_{out} \leq 0.1\%$$

$$T = \frac{1}{f_{sw}} = \frac{1}{100 \text{ kHz}} = 10 \mu\text{s}$$

$$I_{out} = 20.83 \text{ A}$$

$$D_{min} = \frac{V_{out}}{V_{inmin}} = \frac{48}{110} = 0.436 \Rightarrow 43.6\%$$

$$I_{Lsr} = I_{out} = 20.83 \text{ A}$$

$$\Delta i_L = 0.1 \cdot 20.83 \text{ A} = 2.083 \text{ A}$$

$$D_{max} = \frac{V_{out}}{V_{inmin}} = \frac{48}{110 - 0.1 \cdot 110} = \frac{48}{110 - 11} = 0.4848 \Rightarrow 48.48\%$$

$$D_{min} = \frac{V_{out}}{V_{inmax}} = \frac{48}{110 + 0.1 \cdot 110} = \frac{48}{110 + 11} = \frac{48}{121} = 0.396 \Rightarrow 39.6\%$$

a)  $L_c$  - kritična induktivnost.

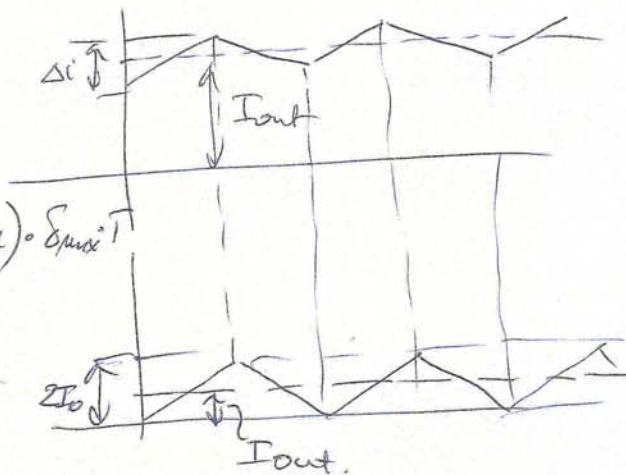
$$(V_{in} - V_{out}) \cdot t_{on} = L \cdot \Delta i$$

$$L_c \cdot 2I_{out} = (V_{inmin} - V_{out}) \cdot D_{max} \cdot T$$

$$L_c = \frac{(V_{inmin} - V_{out}) \cdot D_{max} \cdot T}{2I_{out}}$$

$$L_c = \frac{99 - 48}{2 \cdot 20.83} \cdot 0.4848 \cdot 10 \mu\text{s}$$

$$L_c = 5.93 \mu\text{H} \quad L \gg L_c$$



\* Dimensionierung L

9

$$L \gg \frac{t_{onmin} (V_{inmax} - V_{out})}{\Delta i} = \frac{\delta_{min}}{f_{sw}} \cdot \frac{V_{inmax} - V_{out}}{\Delta i}$$

$$L \gg \frac{0,396}{100k} \cdot \frac{121 - 48}{2,083} = 138,78 \mu H \rightarrow \text{auswahl } L^* = 140 \mu H$$

$$I_{Lmax} = I_L + \frac{\Delta i_L}{2} = I_{out} + \frac{\Delta i_L}{2} = 20,83 + \frac{2,083}{2} = 21,87 A$$

$$L^* = 140 \mu H / 25 A$$

zu messen  $L^* = 140 \mu H$  Tachist diese Pri-  
mity. ml. Nkom se:

$$\Delta i = \frac{\delta_{max} T_o (V_{inmin} - V_{out})}{L^*} = \frac{0,4848 \cdot 10 \mu}{140 \mu} (99 - 48)$$

$$\Delta i = 1,766 A < 2,083 A \quad \checkmark$$

\* Dimensionierung C

$$C \gg \frac{1 - \delta_{min}}{8 L^* f^2 \left( \frac{\Delta V_o}{V_o} \right)}$$

$$\delta_{min} = 0,396$$

$$\frac{\Delta V_o}{V_o} = \frac{0,1}{100} = 0,001$$

$$L^* = 140 \mu H$$

$$f = 100 kHz$$

$$\frac{\Delta V_o}{V_o} = 1m$$

$$C \gg \frac{1 - 0,396}{8 \cdot 140 \mu \cdot (100 \cdot 10^3)^2 \cdot 0,001}$$

$$C \gg 89 \cdot 10^6 \cdot 0,604 = 53,756 \mu F \rightarrow \text{auswahl } C^* = 100 \mu F / 100V =$$

Tachist Nkom Nt Blam zu  $C^* = 100 \mu F$

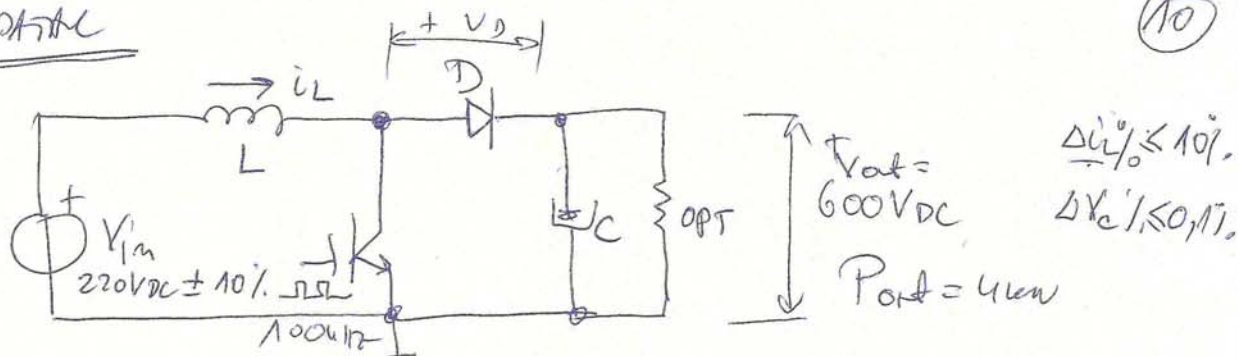
$$\frac{\Delta V_o}{V_o} = \frac{1 - \delta_{min}}{8 \cdot L^* \cdot C^* f^2} = \frac{1 - \delta_{min}}{8 \cdot 140 \mu \cdot 100 \mu \cdot (100 \cdot 10^3)^2} = \frac{1 - 0,396}{8 \cdot 140 \cdot 100 \mu \cdot 10^4}$$

$$\frac{\Delta V_o}{V_o} = 0,00054 = 0,054\% < 0,1\% \quad \checkmark$$



4 ZADANIE

(10)



$$V_{inmax} = 220 + 0,1 \cdot 220 = 220 + 22 = 242V_{DC}$$

$$V_{inmin} = 220 - 0,1 \cdot 220 = 220 - 22 = 198V_{DC}$$

$$198V_{DC} \leq V_{in} \leq 242V_{DC}$$

$$f = 100kHz \Rightarrow T = \frac{1}{f} = \frac{1}{100k} = 10\mu s$$

$$I_{out} = \frac{4000W}{600V} = 6,66A$$

$$R_{out} = \frac{V_{out}}{I_{out}} = \frac{600}{6,66} = 90\Omega$$

$$P_{in} \approx P_{out} = V_{in} \cdot I_{in} = V_{in} \cdot I_{LSE} = 4000W$$

$$I_{LSE} \approx \frac{4000}{V_{in}}$$

$$I_{LSEmax} = \frac{4000}{V_{inmin}} = 20,20A$$

$$I_{LSEmin} = \frac{4000}{V_{inmax}} = 16,52A$$

$$16,52A \leq I_{LSE} \leq 20,20A$$

$$V_{in} \cdot t_{on} = L \Delta i_L$$

$$L_C = \frac{V_{inmin} \cdot t_{onmax}}{2I_O}$$

$$t_{onmax} = ?$$

$$V_{out} = \frac{V_{in}}{1-\delta} \Rightarrow 1-\delta = \frac{V_{in}}{V_{out}}$$

$$\delta = 1 - \frac{V_{in}}{V_{out}}$$

$$\delta_{max} = 1 - \frac{V_{inmin}}{V_{out}} = 1 - \frac{192}{600}$$

$$\delta_{max} = 0,68$$

$$\delta_{min} = 1 - \frac{V_{inmax}}{V_{out}} = 1 - \frac{242}{600}$$

$$\delta_{min} = 0,5966$$

$$t_{onmax} = \delta_{max} \cdot T$$

$$t_{onmax} = 0,68 \cdot 10\mu s$$

$$t_{onmax} = 6,8\mu s$$

$$L_C = \frac{198 \cdot 6,8\mu s}{2 \cdot 20,20} = 33,33\mu H$$

$$L_C = 33,33\mu H$$



b)

\* rezor L

(11)

$$L \geq \frac{V_{in \max} \cdot t_{on \min}}{\Delta i_{L \min}} = \frac{292V \cdot 5,966\mu s}{1,652A} = 880\mu H$$

$$t_{on \min} = S_{\min} \cdot T = 0,5966 \cdot 10\mu s$$

$$t_{on \min} = 5,966\mu s$$

$$\Delta i_{L \min} = 0,1 \cdot I_{L \min} = 0,1 \cdot 16,52 = 1,652A$$

$$\begin{aligned} I_{L \max} &= 20,20A + \frac{\Delta i_L}{2} \\ &= 20,20A + \frac{0,1 \cdot 20,20}{2} \\ &= 20,20A + \frac{2,020}{2} \\ &= 20,20 + 1,010 \end{aligned}$$

$$I_{L \max} = 21,21A$$

msmimo  $L^* = 900\mu H / 25A$

\* rezor C

$$C \geq \frac{I_{out}}{V_{out}} \cdot t_{on} \cdot \frac{1}{\frac{\Delta V_{out}}{V_{out}}}$$

$$t_{on} \rightarrow t_{on \max} = 6,8\mu s$$

$$\frac{\Delta V_{out}}{V_{out}} = \frac{0,1}{100} = 0,001$$

$$C \geq \frac{6,66A}{600} \cdot \frac{6,8\mu s}{0,001}$$

$$C \geq 75,48\mu F \rightarrow \text{msmimo se } C^* = 100\mu F / 1000V \text{ DC}$$

MAX NAPON prelozila Q ze 600VDC → msmta se prelozila ze 1000VDC.

MAX STRA prelozila Q ze 22A → msmta se prelozila ze 25A (50A)

MAX NAPON strze D ze 600VDC → msmta se strze ze 1000VDC

MAX STRA strze D ze 22A → msmta se strze ze 25A (50A)